ODSI's Automated Reservoir and Production Engineering Software

> March 30, 2016 Total - Pau

Chris Fair Oilfield Data Services, Inc. Based on SPE Paper 171512

## Outline

- Intro to Oilfield Data Services (ODSI)
- Bias! & INMP
- Surveillance & Visualization
- Critical Issues for Automation
- Instrumentation by Well Type
- Background Physics for ODSI's Wellbore Model
- Well/Reservoir Analysis Techniques/Tools
- Case Studies
- Conclusions

## **ODSI Consulting Business I**

\* Data Processing, PVT, Rate and Wellbore Modeling

- \* Data QC, Filtering and Condensing
- \* Rate & Water Cut Calculations
- \* Mid-Completion (Datum) BHP Calculations
- \* Well Test & Production Analysis
  - \* PTA/RTA Skin, Perm, P\*, Boundaries, Volumes
  - Static MBAL and Decline Analysis (<u>In-place</u>, <u>Connected</u> and <u>Mobile</u> **HC Volumes**)
  - \* Blind Energy Mapping (don't show us your maps!)
  - \* Damage/Invasion Mapping (do show us your logs!)

## **ODSI Consulting Business II**

#### \* Frac Design/Evaluation

- \* Building Geo-Mechanical Models
- \* Designing the frac to minimize waste
- \* Frac Replay Analysis  $\leftarrow \rightarrow$  Flowback Analysis
  - \* Where did your frac really go?
- \* Post-Job review/optimization

#### \* Remote and On-Site Supervision of Complex Operations

- Job Planning
- Frac Jobs
- \* Exploration DSTs/TSTs

#### **ODSI's Software - Basics**

- \* Operate in "Real-Time" or on Historic Data
- \* Work Within an Operator's Existing Framework
- \* Link to the Database inside the Operator's IT Firewall
- \* Honor the Physics and do the Math in the Background
  - \* Don't Use Correlations
  - \* Don't Force the data to "fit" a model
- \* Do the "grunt" work behind the scenes & do it right!
  - \* Petro-physics, Well Geometry, PVT & Thermal Modeling
- \* Provide Results that Explain a Well's/Reservoir's Performance

#### PRIMARY GOAL: VALID RATES AND VALID BHP!

Secondary Goal: Remove Bias from the Decision-Making Process

#### **ODSI Software – Automated Results**

- \* Calculated Rates and/or Water Cuts
- \* Calculated Datum (mid-completion) BHP
- \* Apparent Oil and/or Water Content in Gas Wells
  - \* DP-PBU
  - \* Re-Injection Cycle
- \* PBU, DD and 2-rate Well Test Interpretation
  - \* Skin, Perm, Productivity, Completion Efficiency; P\*
- \* Static MBAL & Decline Analysis
  - \* In-place, Hydraulically Connected & Mobile HC Volumes
  - \* Relative Productivity/Relative Inverse Productivity

#### Bias, Bullies & "It's not my Problem"

## **Bias in Decisions**

- Confirmation/Expectation Bias
  - Decision Already Made
  - Answer Already "given"
- The Inside View
- Risk Compensation
- Gambler's Fallacy
- Ownership/Sunk Cost Bias
- Unintended Consequences Incentives
- Gotta Spend it...(budgets)

#### Turds in the Pool

- \* The "Expert"
- \* The "Smartest Guy in the Room"
- \* The Information Hoarder
- \* The Bully
- \* The Grenade Tosser
- \* The Hold-out
- \* The Amateur Epidemiologist
- \* Mister Minutia
- \* The Investment Banker

#### Whose Problem is it?

- \* Drilling: We got the hole down it's not my problem
- \* Completions: The well flowed it's not my problem
- \* Frac'ing: We pumped all the sand INMP
- Facilities: I designed it for what you told me the rate was going to be - INMP
- \* Production: Not a wellbore or skin problem see my nodal
- \* Reservoir: It's not a perm/Vc issue see my nodal
- Geology/Exp: It HAS to be big! Must be someone else's fault/problem
- Geo-physics: The interpreted log says it's HC bearing the water must be coming from somewhere else

## Well...

- Drilling: Fluid Type/Losses can induce damage
- Completions: Fluid Type/Losses, Completion Type and Execution affect performance
- Frac'ing: If you frac out of zone or the proppant gets crushed, your frac may not be any good
- \* Facilities: Do the best you can with what you have
- \* Production/Reservoir: Find the pressure drop that shouldn't be there!
- \* Geology/Exp: Communicate with RE How big is it?
- \* Geo-physics: Try digging up the 'raw" \*.las data; don't assume that the service co. "interpreted" it correctly

## It's Everybody's Problem

- \* Understand what happened in the Past
- \* Understand what's happing Now
- \* Get an idea of what's going to happen in the Future

Need Non-Biased (non-bullying) way to sort things out

#### What is Good Surveillance?

#### \* Always have a handle on:

- \* How much oil or gas is in the ground
- \* How much of it is likely to be recovered
- \* What is the current well performance? Can anything be done to improve the performance?
- \* Are there problems developing in the well bore?
- \* Are there problems developing in the completion?
- \* Are there problems developing in the reservoir?
- \* Is anything changing?
- \* If something happens, what is the current NPV of the asset?

#### What is Bad Surveillance

- Only accept information about the well/reservoir that fits your or the company's beliefs
- \* Change the "static" or geologic model until you get the answer you want
- \* Wait until something bad happens:
  - \* Call it bad luck & move on
  - \* Say it's too late to fix it & move on
  - \* Call in a technical expert & move on
  - \* Use Nodal Analysis or Simulation to muddy the waters
- \* Be reactive... or just do nothing

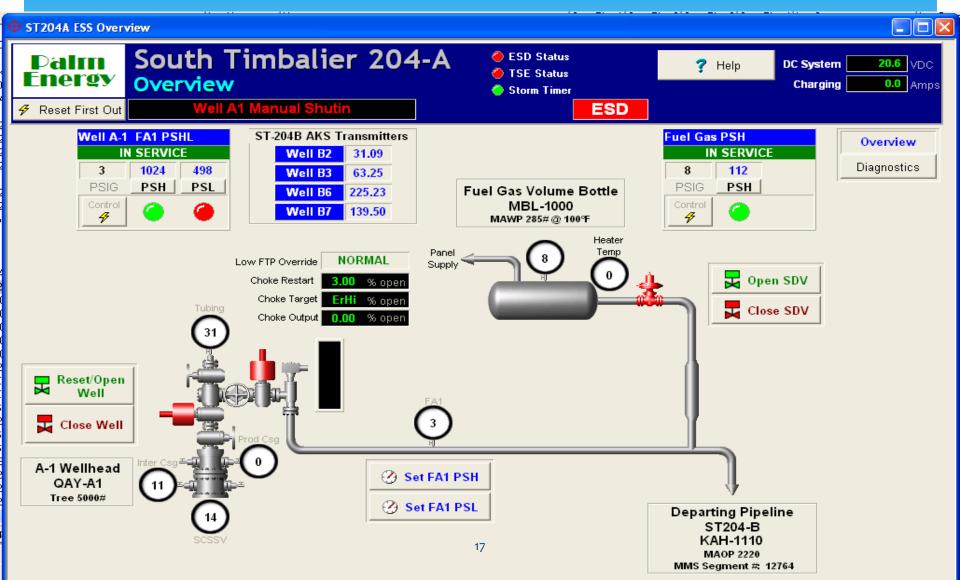
#### **Current Surveillance Programs**

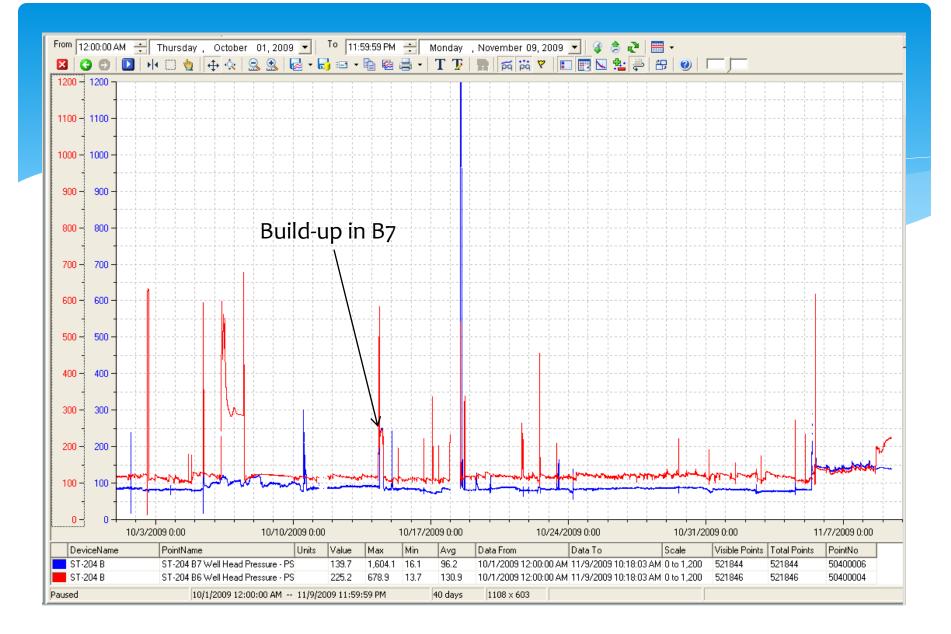
- \* Some Operators STILL don't even have Scada
- \* Some have Scada, but no data visualization
- \* Some have Scada & Visualization, but only for some departments
- \* Some have alarms, triggers, automatic PBU recognition
- Some have links to internal & external software packages

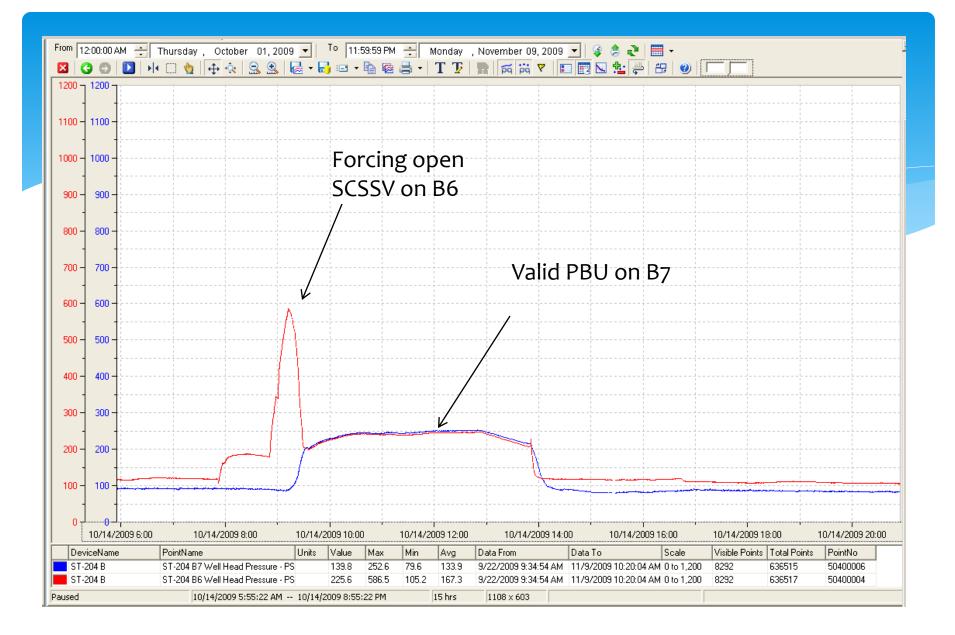
## Drowning in Data?

- Engineers doing surveillance work spend over half their time just looking for data
- Many data systems are still designed as if computer storage/memory were expensive
- Many software packages cannot handle multi-million point data sets
- \* Need a common framework that engineers and managers can use and understand & visualize!

#### **Data Visualization**







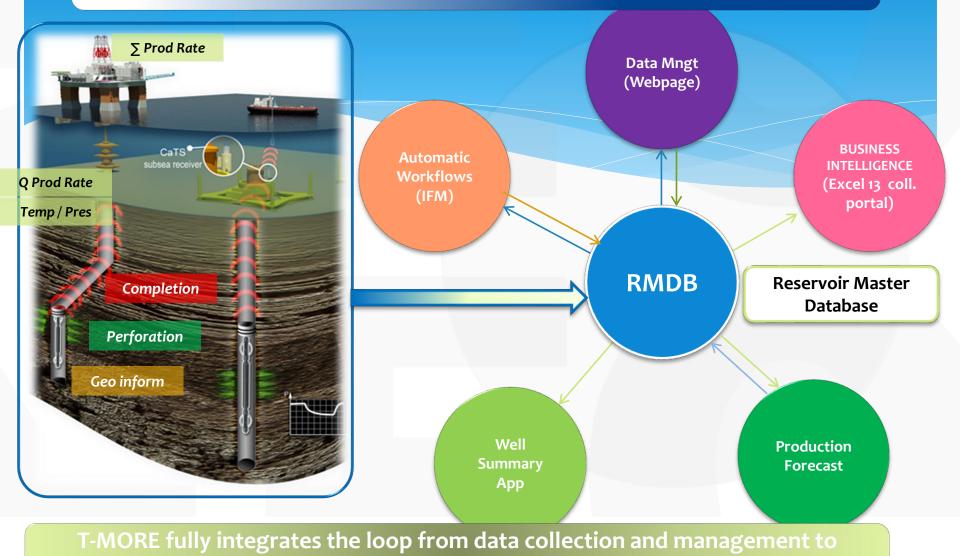
#### **Common Framework - Basics**

- \* Easy Access to Data
- Ability to do diagnostic graphs, with annotations
- \* Links to Email
- \* Process Alarms
- \* Ability to Plug & Play with other software packages, not just the Framework's software

This forms the basics for Automated Real-Time Analysis!

## Total's Solution: T-MORE

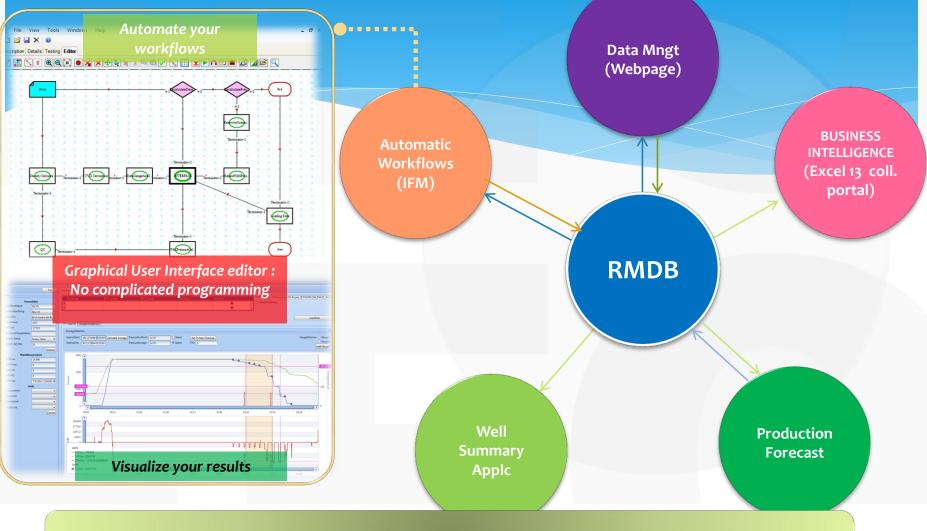
#### **T-MORE** → DATABASES AND INTERFACES



Reservoir management processes

#### Where Does ODSI Fit in this Set-up?

#### **T-MORE** → DATABASES AND INTERFACES



#### **AUTOMATE YOUR RESERVOIR WORKFLOWS**

#### **ODSI-PI (or T-MORE)** Interface



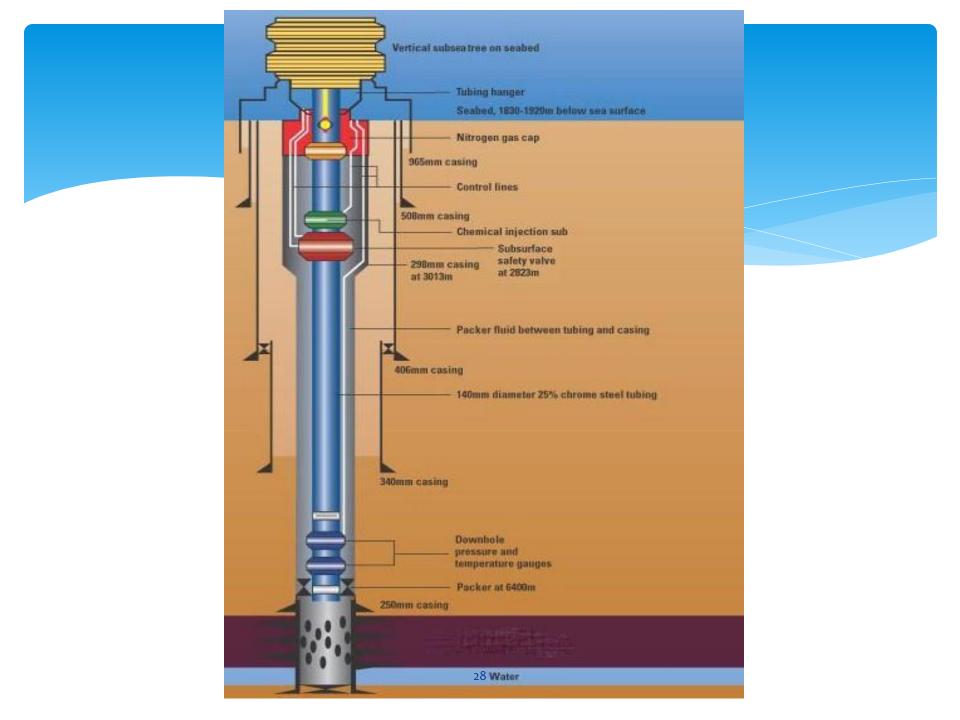
- ODSI's Windows Service is installed on the PI Server, inside the firewall
- ODSI WS Reads the PI Tags it needs to perform the calculations
- ODSI WS then Writes the Results of the Calculations back to PI
  - Qgas, BHP, Perm, Skin, P\*, PI, etc.
- These calculations are then available for IFM to utilize
- Automated Reports (Well Test Analysis, Decline Analysis, Static MBAL) are Written to a Shared Folder within the Network
- Digital Versions of the results are maintained in a \*.csv file
- Engineers and T-MORE can access results, reports and summary files through IFM or a dedicated T-MORE/ODSI interface

#### **Critical Issues for Automation**

- \* Instrumentation Quality & Location
- Data Source, Data Acquisition Frequency, and Data Storage (dead-banding!!!)
- \* Well/Completion Type (every well is different)
- \* Reservoir "Signal" Rate of Change in Pressure
  - \* The higher the kh, the smaller the "signal"
- \* Operationally Dependent Items
  - \* How is the well shut-in (Staged?)
  - \* How is the well brought on production (Stepped?)
  - \* How is the well produced (steady, swing?)
- \* How is rate "measured" or calculated?

## Instrumentation by Well Type

- Possible Instrumentation (Upstream of Facilities)
- \* Instrumentation based on well type:
  - \* Natural Flow Gas & Gas/Condy
  - Natural Flow Oil
  - \* Artificial Lift Oil
  - \* Annular Flow Wells (CBM/CSM)
  - Water Injection
  - \* Nat Gas injection
  - CO2 injection
  - \* Steam Injection



#### Pressure/Temperature Measurement

# What do I really need to measure accurately?

- \* Wellhead Pressure
- \* Wellhead Temperature (Thermowell)
- \* Downhole Pressure
- \* Downhole Temperature
- \* Distributed Temperature (multi-zone wells)
- \* Line Pressure/Temperature
- \* Annular Pressures

#### Rates and Valve/Ck Status

#### \* Flow Rates of Oil, Gas & Water

- \* Multiphase Meters, Venturi Meters, Turbine Meters, d/p meters (Daniels), Coriolis meters, Ultrasonic Flowmeter
- \* Dedicated Test Separator
- \* Meter Prover
- \* Virtual Rate Measurement (VRM)... based on what?
- \* Other bits
  - \* Choke Setting
  - \* SCSSV, MV, Control Valves
  - Injection lines

## Instrumentation Needs Based on Well Type

# Basics: What do you need to evaluate your well/reservoir?

- \* Way to get Qgas, Qoil & Qwater
- \* Way to get Mid-Completion BHP
- \* Temperatures, Choke & Valve Settings are nice too!

## Gas & Gas/Condy Wells

- Need at least one pressure and continuously measured Rates...OR
- Two pressures in/on well (can be used to calculate gas rate)
- \* Choke Setting
- \* Valve Status
- \* MPFM?

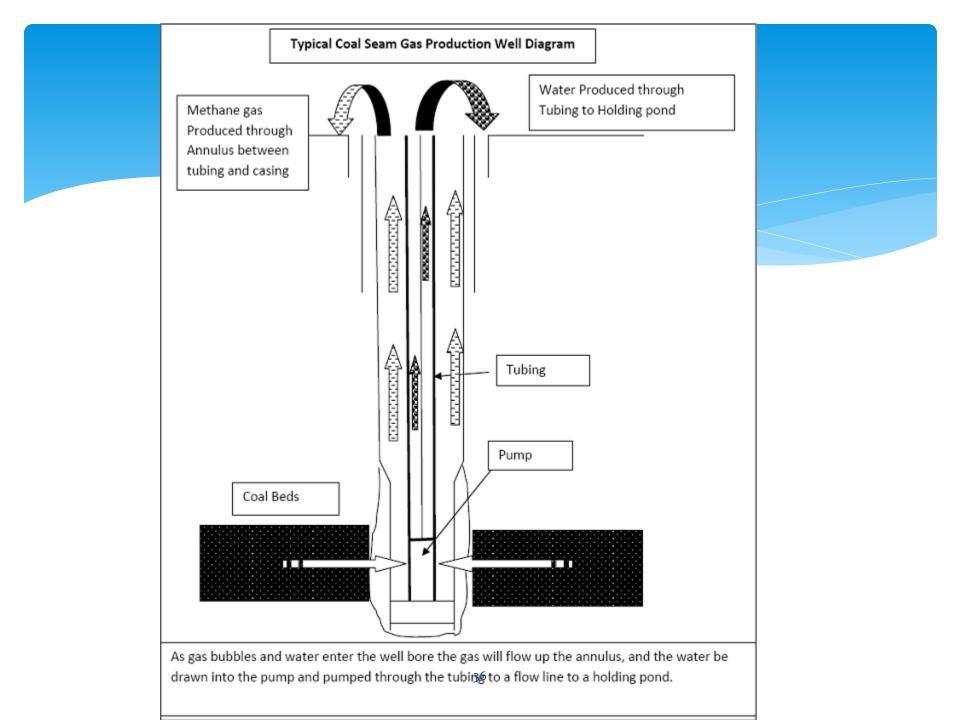
Note: If well is expected to make significant water or if the free Condensate yield is above 30 bbl/MMcf – dhgs are recommended

## Naturally Flowing Oil Wells

- \* Tree & DHG (Pressure & Temperature)
  - \* Can be used to calculate water cut
- \* Mass Flowmeter, Turbine Meter, MPFM, Integrated Tank Level flow indicator
- \* Choke Setting
- \* Valve Status

## Artificial Lift Oil Wells

- Same as natural flow, but DHPG must be below the artificial lift system (and Tree pressure may be irrelevant)
  - Below pump for PCP, ESP or jet pump (in communication with reservoir)
  - Below standing valve for sucker-rod
  - Below mandrel for gas lift (+gas injection pressure)



# Annular Flow (CSM)

- \* Annulus Pressure/Temperature
- \* WHT/WHP
- \* Pump torque & rpm
- \* DHG (below pump)
- \* Liquid Level indicator (avoid running pump dry)
- \* Water Rate (tubing) tank level meter
- \* Gas Rate (annulus)

## Water Injectors

- \* DHG Pressure/Temperature
- Can use WHP if well doesn't go on vacuum during falloff
- \* Qwater (turbine meter)
- \* Ways to measure/infer water gravity
  - \* Capacitance
  - \* Salinity
  - \* Density

## Nat Gas, CO2 & Steam Injectors

- If composition is constant, can get by with just WHP and Qgas-inj and Tinj
- \* If composition is variable or well is a recycler, need WHP, WHT, DHGP, DHGT and Qgas (mass flow)
- \* Valve Status
- \* Choke Status
- \* For CO2 Injectors: DHG and Tree gauge required
  - \* PVT tuning & rate validation
- \* For Steam Injectors: Same as nat gas inj.

### **Comments on Instrumentation**

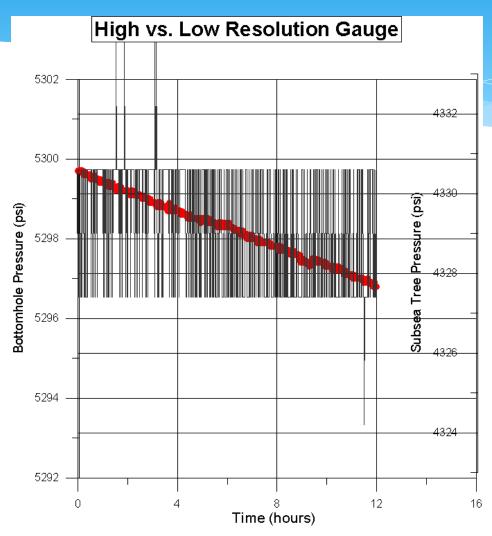
- \* Instrumentation is relatively cheap
  - Price difference between good and crap equipment is small
  - \* Cable (TEC) and Rig Time are not
- \* Don't drop bits!
  - \* Most transmitters are 18-24 bit
  - \* Don't lose resolution over a \$30 vs. a \$50 I/O card

#### \* Let the end users spec the equipment!

#### Data Transfer: Don't Lose Resolution!

- Before it gets to you, Your Data is likely to pass through:
  - \* One or two A/D converters
  - \* An I/O card on the Control Panel
  - Dead-band filters
  - \* Signal filters
  - \* Archive filters
- \* You can lose sampling resolution (frequency) and instrument resolution at any point along the way

## Don't Lose Resolution!



How Do We Make Use of Automated Surveillance?

... may have to change the way we work and assign responsibility

#### One Last Form of Bias...

## **Automation Bias!**

## How to "Bird-Dog" a Well Production problem

- \* Is it a wellbore problem?
  - \* Scale/Wax/Asphaltenes, Loading, Parted String
- \* Is it a completion problem?
  - \* Skin Accretion, Screen Plugging, Completion Failure
- \* Is it a reservoir problem?
  - \* Perm?
  - \* Reserves?
  - \* Water Encroachment?
- \* Is it a combination of two or more of the above?

FIND THE PRESSURE DROP THAT SHOULDN'T BE THERE!

#### Remember: Every Well is Different!

- \* Well Geometry
- Completion type
- \* Data Source/Instrumentation
- \* Data Frequency & Management
- \* How Many Reservoir Layers?
- \* Reservoir Signal (how "flat" is the build-up?)
- \* Wellbore Lift Mechanism
- \* Reservoir Drive Mechanism
- \* How is the Well Operated?

#### Each Well's Data Acquisition Strategy Needs to Consider All of These Items

Reservoir & Production Engineering Analysis/Evaluation Tools

What they are and what they tell you

#### Analysis Types and Their Objectives

- \* PTA (Pressure Transient Analysis)
  - \* Skin, Perm, Deliverability, Communication, Productivity, Reservoir Boundaries, Reserves, Reservoir Pressure (P\*)
- \* RTA (Rate Transient Analysis)
  - \* Same as PTA, but with less reliability on boundaries
- \* P/z Plots (gas) & Static MBAL Plots (oil)
  - \* Oil and/or Gas in Place
- \* Decline Analysis: Flowing BHP or IP vs Time
  - \* Apparent HC Volumes Running MBAL/EBAL
- \* Nodal Analysis: Interaction of WB/Comp/Res
  - \* Changes in well performance; short-term rate predictions
- Reservoir Simulation: Cell/Gridblock disposition of Saturations, Pressures (Energy)
  - \* Field Optimization; longer-term rate/withdrawal predictions

## Analysis Type Examples

- \* Build-up PTA Derivative
- \* Drawdown PTA Semilog
- \* Horner P\*
- \* Proper RTA (Rate Transient Analysis)
- \* MBAL/EBAL "bookends"
- \* P/z (gas) or Static MBAL (oil)
- \* Conventional Decline Analysis (Running MBAL)
- \* TTA/IPA (Running EBAL)
- \* NODAL ANALYSIS
- \* Simulated Rates/Pressure vs. Actual

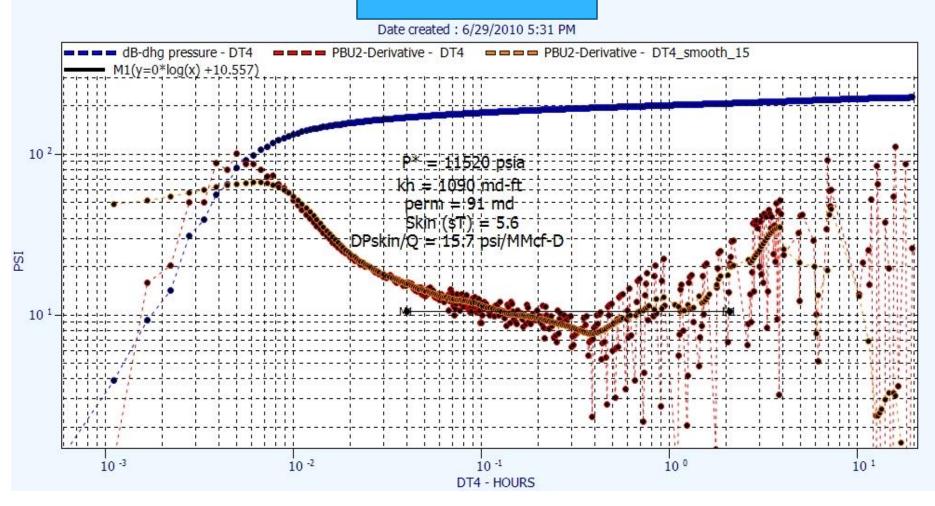
## Analysis/Evaluation Tools: PTA

- Build-up: After flowing the well for a while, shut it in and observe the pressure response
  - \* If Long Enough, Valid P\*
- Drawdown: After shutting in the well for a while, flow it on a constant choke and observe the pressure and rate response
- 2-rate: Change the rate enough to create a new transient; observe P & Q
- \* Multi-rate: Change the rates and compare DP vs Q
- Communication: Shut-in a well and see if a neighboring well causes the Pressure to drop

## Build-up PTA

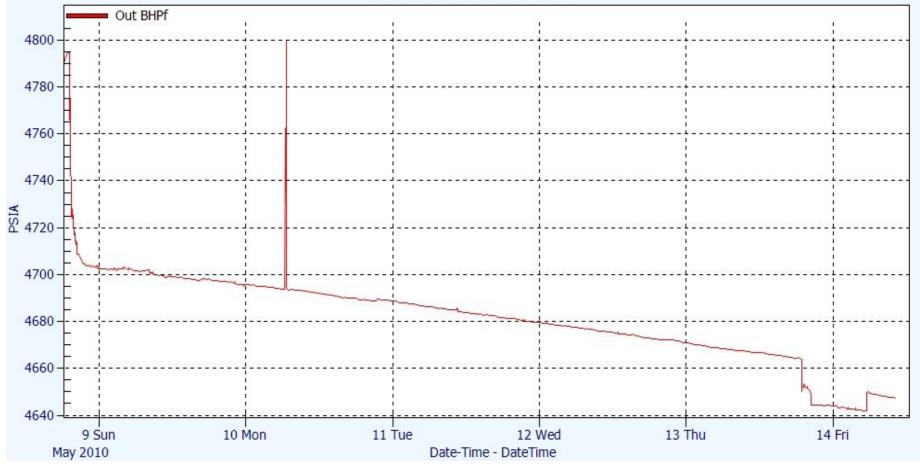


## **Build-up Derivative Analysis**

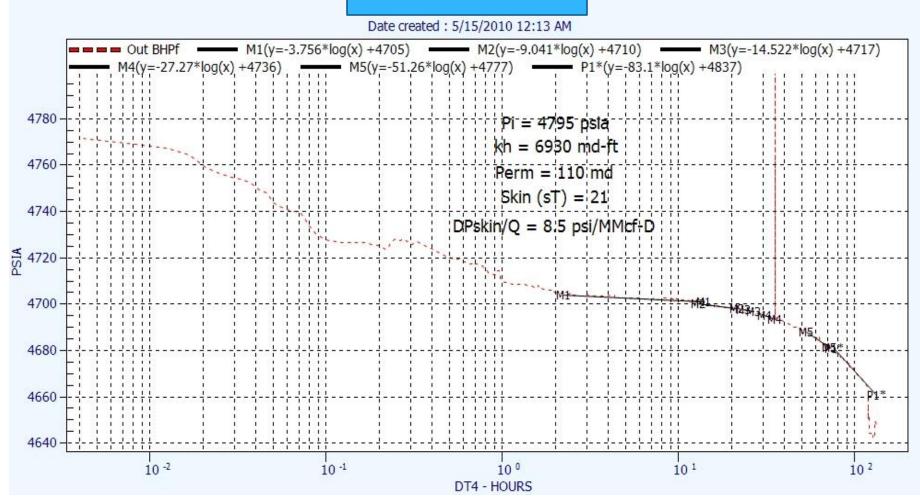


#### Drawdown - PTA

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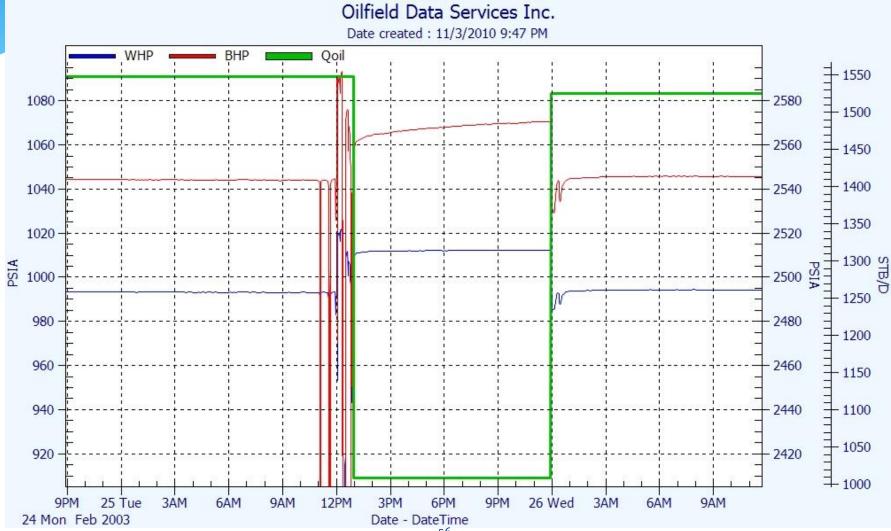
## Drawdown PTA - Semilog Analysis



#### Horner Plot – P\* Determination



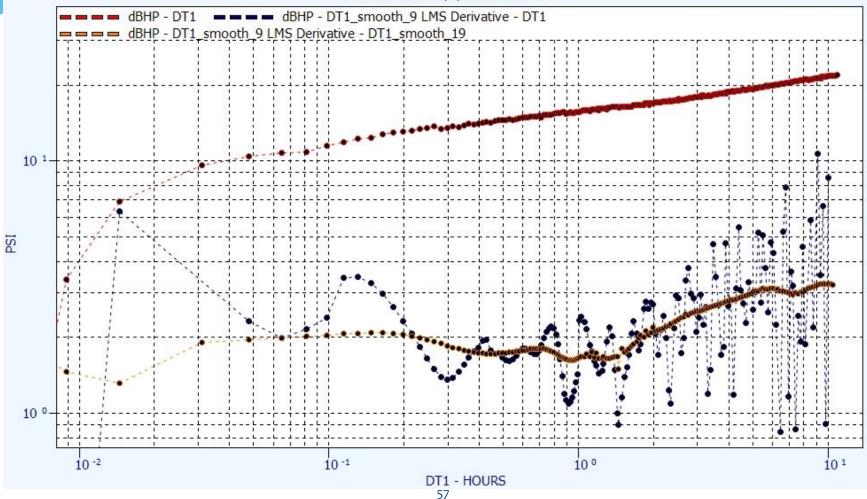
## 2-Rate Test (Esp. for Oil)



## 2-Rate Derivative (Oil)

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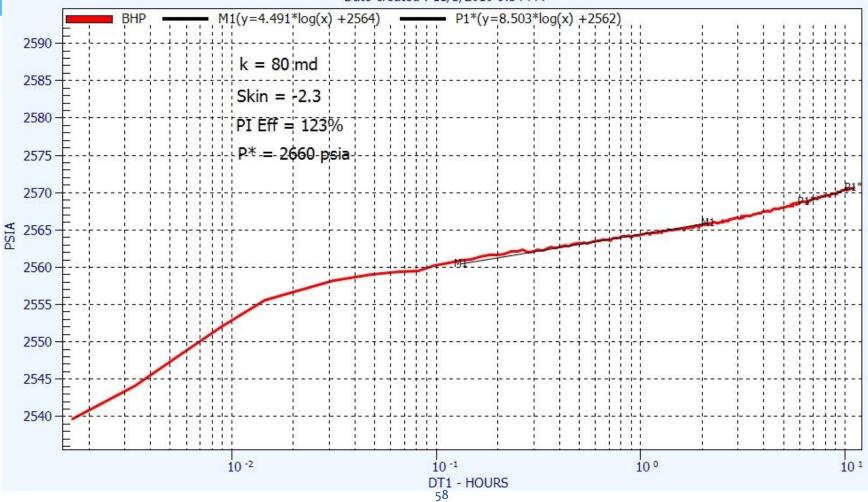
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## 2-Rate Oil Semilog

#### Oilfield Data Services Inc.

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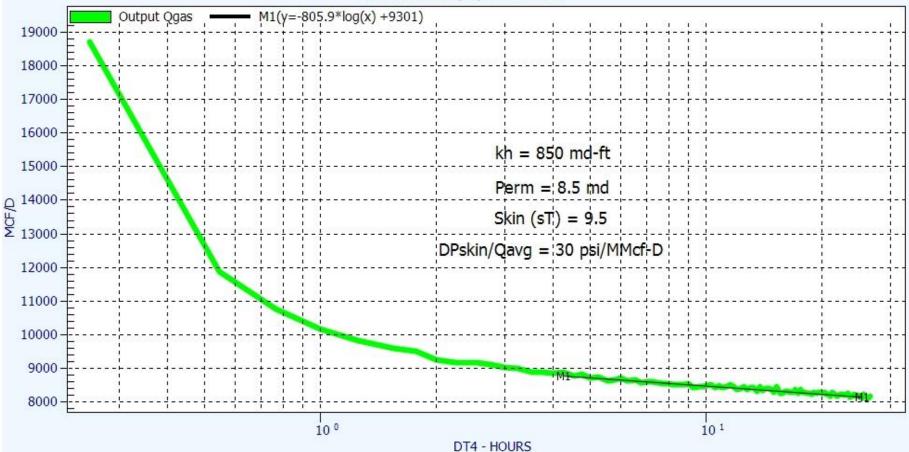


#### **RTA Example - Cartesian**



## RTA – Semi-log Analysis

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## Two Simple Bookends: Applied to Static and Dynamic MBAL/EBAL

- \* Expansion Drive Only (Compressibility Volume)
   \* Vc
- \* Infinite Water Drive Only (Pushed Volume)
  - \* Vsld

## P/z & Static MBAL

- \* Static MBAL for Oil Conventional & SLD
  - \* Conventional: N = Np \* Boi/(Bo|Np Boi)
  - \* SLD: N = Np\*Pi/(Pi-P|Np)
- \* Static MBAL for Gas Conventional & SLD
  - \* Conventional: G = Gp\*Bgi/(Bg|Gp Bgi)
  - \* SLD: G = Gp\*Pi/(Pi-P|Gp)
- \* P/z for Gas: Plot P\* vs Gp and P\*/z vs Gp
  - \* SLD In-place = Intercept of P\* slope at 15 psia
  - \* P\*/z In-place = Intercept of P\*/z slope at 15 psia

Where Bo|Np or Bg|Gp are FVFs at current Preservoir coincident with the produced hydrocarbon volume and P|Np or P|Gp are the current reservoir pressure

## Conventional & TTA Decline

- \* Conventional Decline Relates to Hydraulically Connected Volume
  - \* DP-DT Slope is the Conventional decline slope
- \* TTA Decline Relates to Mobile Volume
  - \* The TTA function is simply the relative inverse productivity: (*Pinitial-Pwf*)/Qspot
  - \* Slope is the TTA-slope

## **Conventional Decline Analysis**

\* ConVc = Qavg/(DP/DT-slope\*Ct)

\* ConV<sub>SLD</sub> = Qavg\*Preservoir/(DP/DT-slope)

 $V_{SLD}$  and Vc = volume in units compatible with Qavg & DT, Qavg [=] average flow rate over the period where the DP/DT-slope is selected, DP/DT-slope is the decline in pressure per unit time [=] psi/day, and Ct is total system compressibility (1/psi).

## **TTA Decline Analysis**

- \* TTA|Vc = 1/(TTA-Slope\*Ct)
- \* TTA V<sub>SLD</sub> = Preservoir/TTA-Slope

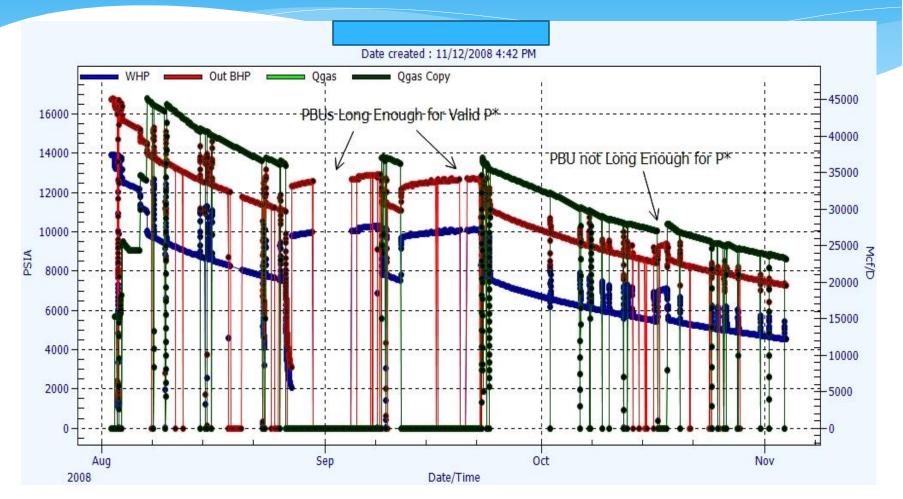
TTA-Slope has units consistent with the stock-tank or standard condition rate units and pressures

### Six Values:

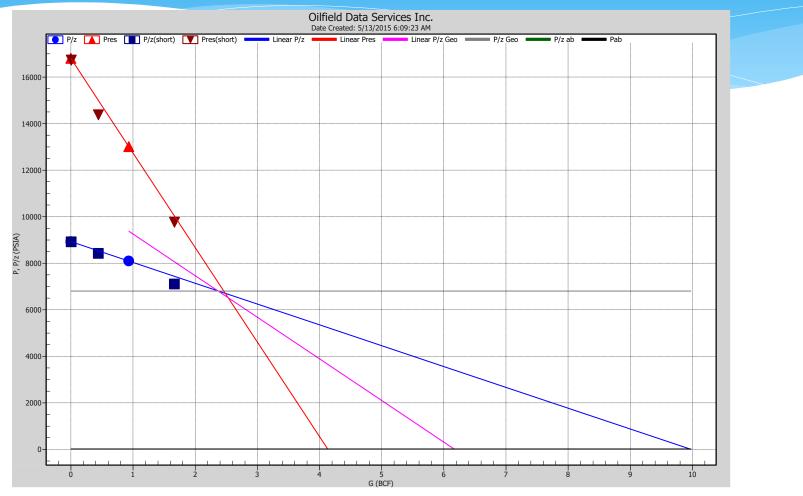
- \* Static MBAL (expansion) In-place Energy
- \* Static MBAL (SLD) Pushed In-Place Energy
- \* Conventional Vc Hydraulically Connected Energy
- \* Conventional SLD Pushed Hyd. Conn. NRG
- \* TTA Vc Mobile Energy
- \* TTA SLD Pushed Mobile Energy

Changes in these values Mean Something!!!

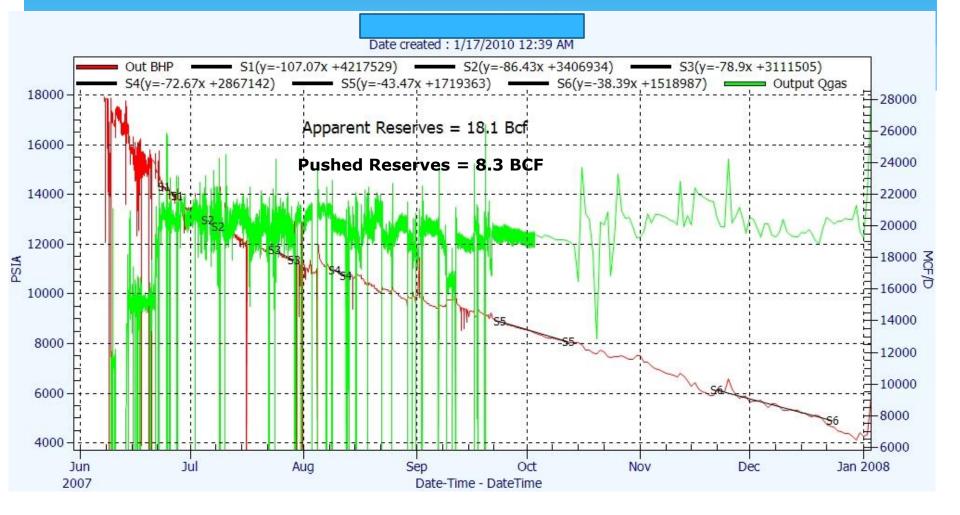
## Production History for P/z



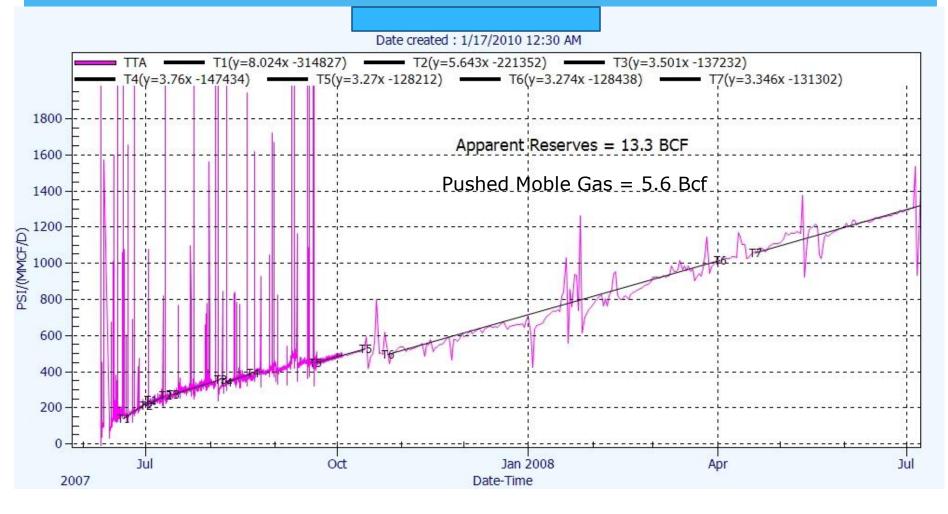
## P/z Example



#### **Conventional Decline Evaluation**



## TTA "Decline" Analysis



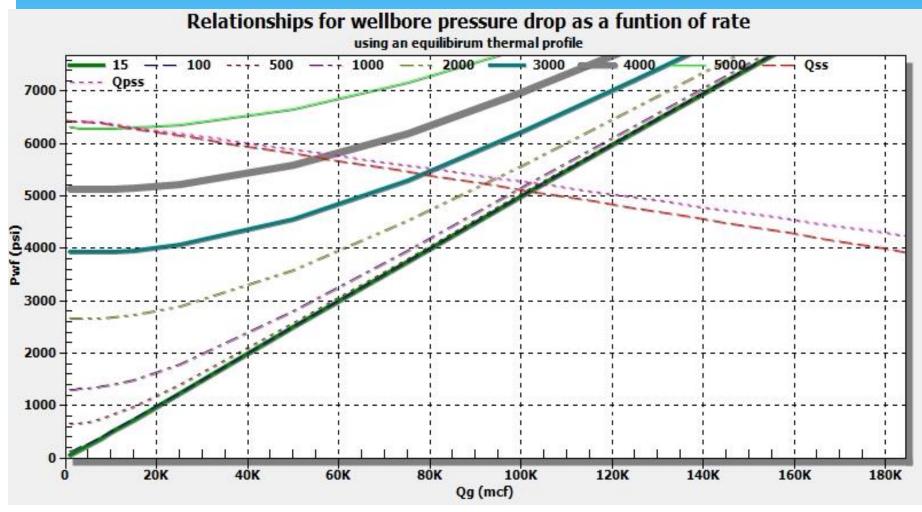
## "Static" Nodal Analysis

- Compares Reservoir Inflow (IPC) with Wellbore Performance (VLP)
  - \* Allows Prediction of DP to achieve a Rate (vice versa)
  - \* Allows Prediction of Liquid Loading Scenarios
  - \* Allows Optimization of Tubular Design
- \* Problems with Nodal
  - Infinite # of combos of skin & perm calculate the same rate (Can't use nodal to determine skin or perm)
  - User has to pick the right inflow model and right VLP correlation
  - Doesn't handle transient situations well may match your well today, but not next month

## Nodal – IPC + VLP

|             | File Men        |      | lysis Plot View      |              | 0\nodal out2.ProData - [WellboreDe<br>Heln | aiverabilityDialogj   |           |                   |                |                |                   |                                |                   |                |            |          |                | - 8               |
|-------------|-----------------|------|----------------------|--------------|--|---|-----------|-------------------|----------------|----------------|-------------------|--------------------------------|-------------------|----------------|------------|----------|----------------|-------------------|
|             | Gas Rate        | -    | C Inflow             | Inputs       | Units                                      | A   | 100       | 500               | 1000           | 2000           | 3000              | 4000                           | 5000              | I              | J          | к        | L              | M                 |
| _           | 2000            | 100  | PSTAR                | 6500         | psi  | 25000   | 1239.9    | 1393.3            | 1794.8         | 2892.1         | 4070.1            | 5230.4                         | 6363.2            |                |            |          |                |                   |
| -           | 3000            | 500  | Max Pwf              | 6500         | psi  | 50000   | 2500.0    | 2579.0            | 2812.0         | 3588.2         | 4563.2            | 5602.3                         | 6658.5            |                |            |          |                |                   |
| -           | 4000            | 1000 | Pwf Step             | 100          | psi  | 75000   | 3759.1    | 3810.6            | 3966.8         | 4530.4         | 5313.2            | 6210.0                         | 7163.8            |                |            |          |                |                   |
| -           | 5000            | 2000 | Perm                 | 10           | md   | 100000  | 5000.7    | 5038.1            | 5153.0         | 5583.3         | 6217.2            | 6983.2                         | 7830.9            |                |            |          |                |                   |
| _           | 6000            | 3000 | Skin                 | -1.5         |  | 125000  | 6227.1    | 6256.1            | 6345.7         | 6688.4         | 7211.7            | 7867.9                         | 8617.5            |                |            |          |                |                   |
|             | 7000            | 4000 | D                    | .0000001     | 1/mcf                                      | - 150000  | 7449.3    | 7472.8            | 7545.4         | 7826.9         | 8266.8            | 8833.2                         | 9496.2            |                |            |          |                |                   |
|             | 8000            | 5000 | Time                 | 24           | Hours                                      | 175000  | 8676.9    | 8696.4            | 8757.0         | 8993.7         | 9369.5            | 9862.5                         | 10450.8           |                |            |          |                |                   |
| -           | 10000           |      | Radius Override      | F            |  | 200000  | 9862.5    | 9879.3            | 9931.5         | 10136.5        | 10465.2           | 10901.9                        | 11430.0           |                |            |          |                |                   |
| 0           | 15000           |      | Radius               | 0            | ft   | 250000  | 12211.7   | 12224.7           | 12265.4        | 12426.1        | 12687.2           | 13039.9                        | 13474.3           |                |            |          |                |                   |
| 1           | 25000           |      | rw                   | 0.350        | ft   | 250000  | 12211./   | 1222-1.7          | 12205.1        | 1212011        | 12007.2           | 15055.5                        | 1047410           |                |            |          |                |                   |
| 2           | 50000           |      | Net TVT Pay          | 120.0        | ft   | Pwf   | 6400.0    | 6300.0            | 6200.0         | 6100.0         | 6000.0            | 5900.0                         | 5800.0            | 5700.0         | 5600.0     | 5500.0   | 5400.0         | 5300.0            |
| 2           | 75000           |      | Porosity             | 0.11         |  | Qss   | 7294.4    | 14587.5           | 21878.7        | 29167.3        | 36452.6           | 43733.7                        | 51009.9           | 58280.2        | 65543.6    | 72799.2  | 80045.8        | 87282.3           |
| 3<br>4      | 100000          | 1    | Sw                   | 0.11         |  |   | 8252.4    | 14587.5           | 24754.7        | 33003.2        | 41248.8           | 49490.7                        | 57728.0           | 65959.6        | 74184.5    | 82401.6  | 90609.7        | 98807.5           |
| .4<br>.5    | 125000          |      | So                   | 0.22         |  | Qpss  | 6449.9    | 16504.2<br>6399.5 | 6348.8         | 6297.9         | 41248.8<br>6246.7 | 49490.7<br>6195.2              | 57728.0<br>6143.4 | 6091.2         | 6038.8     | 5986.1   | 5933.0         | 98807.5<br>5879.6 |
| 16          | 125000          |      | Sg                   | 0.00         |  | Pavg  | 1008.1    | 1004.0            |                |                | 991.6             | 987.3                          |                   |                | 974.4      | 970.0    |                |                   |
| 6<br>7      | 150000          |      | Sg<br>Cf             | 0.78<br>4.67 | microsips                                  | -   | 0.028     | 1004.0            | 999.9<br>0.028 | 995.8<br>0.028 | 991.6<br>0.028    | 987.3                          | 983.1<br>0.027    | 978.8<br>0.027 | 9/4.4      | 970.0    | 965.6<br>0.027 | 961.1<br>0.027    |
|             |                 |      |                      |              |  | mu  |           |                   |                |                |                   |                                |                   |                |            |          |                |                   |
| 8           | 200000          |      | Plot ?               | Qss          | ✓ Qpss                                     | В   | 0.642     | 0.645             | 0.648          | 0.652          | 0.655             | 0.658                          | 0.662             | 0.665          | 0.669      | 0.673    | 0.677          | 0.681             |
| 9           | 250000          |      | WCD Pwf<br>Calculate | 4950         |  | eta<br>₹ ∢  | 10585.865 | 10500.499         | 10414.714      | 10328.504      | 10241.863         | 10154.787                      | 10067.268         | 9979.300       | 9890.876   | 9801.990 | 9712.633       | 9622.79           |
| Depti       | h: 60<br>h: 210 |      |                      |              | Depth: 18                                  | [   | 15<br>Qss | 10                |                | us             |                   | e pressur<br>ilibirum th<br>20 |                   |                | tion of ra |          | 5000           |                   |
| 20<br>Depti |                 |      |                      |              | Depth: 18                                  | [   |           | 10                | 0              | us             | ing an equ        | ilibirum th                    | ermal prof        | ile            |            |          | 5000           |                   |
| Dept        |                 |      |                      |              | Depth: 18                                  | 0 7000 -<br>6000 -  |           | 10                | 0              | us             | ing an equ        | ilibirum th                    | ermal prof        | ile            |            |          | 5000           |                   |
| Dept        |                 |      |                      |              | Depth: 18                                  | 0 7000 -<br>6000 -<br>5000 -<br>(10 4000 -<br>2000 -                                    |           | 10                | 0              | us             | ing an equ        | ilibirum th                    | ermal prof        | ile            |            |          | 5000           |                   |
| Deptl       |                 |      |                      |              |  | 50 7000 -<br>6000 -<br>5000 -<br>5000 -<br>3000 -<br>3000 -<br>2000 -                   |           | 10                | 0              | us             | ing an equ        | ilibirum th                    | ermal prof        | ile            |            |          | 5000           |                   |
| Dept        |                 |      |                      |              |  | 50 7000 -<br>6000 -<br>5000 -<br>5000 -<br>2 4000 -<br>2 4000 -<br>2 4000 -<br>2 4000 - | 0,955     | 10                | 0              | us             | ing an equ        | nilibirum th                   | ermal prof        | ile            |            |          | 5000           | 180K              |

#### Nodal VLP-IPC Plot



#### Transient Nodal Analysis Tool

- Keep track of changing produced fluid composition
- \* Update skin & perm from last valid PTA
- \* Update P\* from last valid PBU
- \* Keep track of pressure decay during drawdown
  - \* Adjust Preservoir while producing
  - \* Use Transient Inflow model when in transient flow
  - Use Appropriate Steady State Inflow model when in SS Flow
- \* Link Reservoir Simulator to Wellbore Model

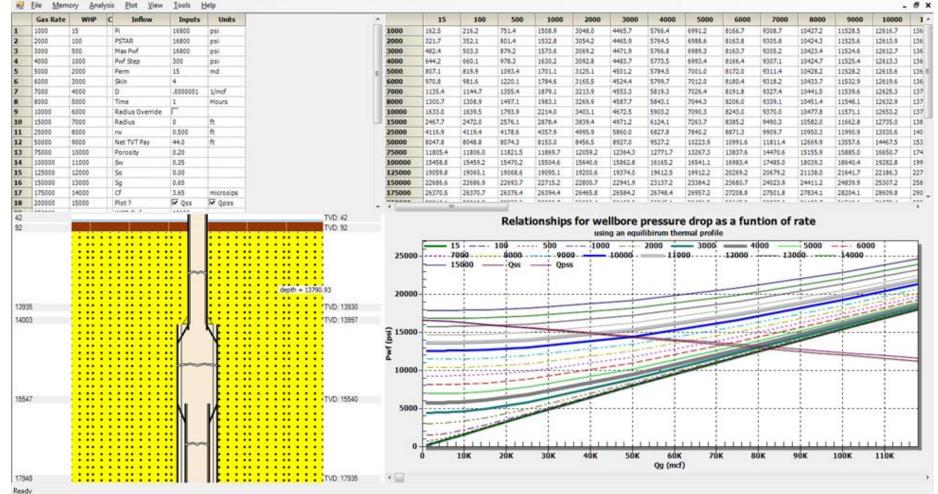
#### **Transient Nodal Initiation**

- \* Preservoir, Treservoir
- \* Skin (s & D) & Perm from Flowback PTA
- \* Wellbore Radius and Net TVT pay
- \* Fluid PVT
- \* Well Configuration/Geometry
- Petro-physical inputs
  - \* Sw, porosity, formation compressibility
- Forced Fixed Reservoir Volume or Floating Reservoir Volume
- \* Production Time Since last Valid P\*/Pres

#### **Nodal Initiation Run**

#### no obsi-Well Analyzer - C./Users/Chris/Downloads/RT Software Demos/GOM Reserves RT Trial v Jan 18 ProData - [WellboreDeliverabilityDialog]

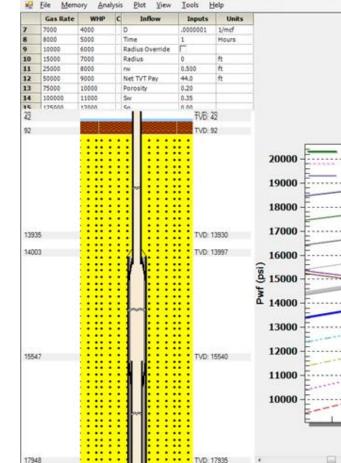
0 0 ×



#### Inflow and VLP for Tp = 1 hour

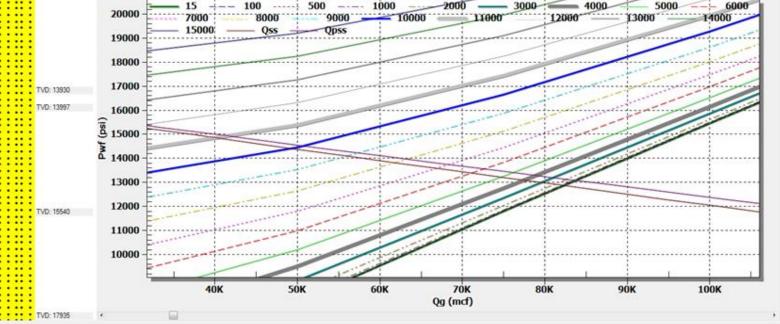
#### n ODSI-Well Analyzer - C/Users/Chris/Downloads/RT Software Demos/GOM Reserves RT Trial v Jan 18 ProData - [WellboreDeliverabilityDialog]

0 8



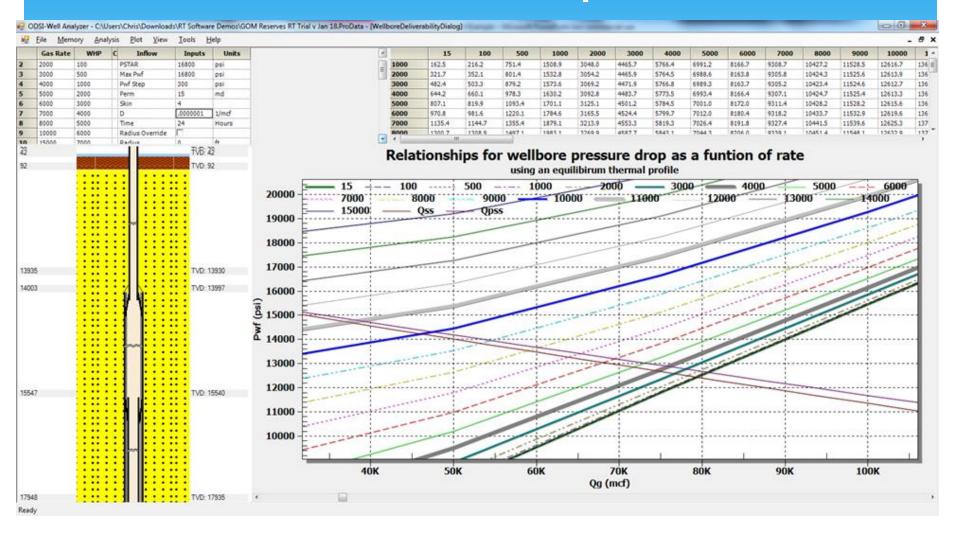
| _   |      |        |        |        |        |        |         |         |        |        |        |         |         |         | -     |
|-----|------|--------|--------|--------|--------|--------|---------|---------|--------|--------|--------|---------|---------|---------|-------|
| · · |      | 15     | 100    | 500    | 1000   | 2000   | 3000    | 4000    | 5000   | 6000   | 7000   | 8000    | 9000    | 10000   | 1.4   |
|     | 1000 | 162.5  | 216.2  | 751.4  | 1508.9 | 3048.0 | 4465.7  | 5766.4  | 6991.2 | 8166.7 | 9308.7 | 10427.2 | 11528.5 | 12616.7 | 136 1 |
|     | 2000 | 321.7  | 352.1  | 801.4  | 1532.8 | 3054.2 | 4465.9  | \$764.5 | 6988.6 | 8163.8 | 9305.8 | 10424.3 | 11525.6 | 12613.9 | 136   |
|     | 3000 | 482.4  | \$03.3 | 879.2  | 1573.6 | 3069.2 | 4471.9  | \$766.8 | 6989.3 | 8163.7 | 9305.2 | 10423.4 | 11524.6 | 12612.7 | 136   |
|     | 4000 | 644.2  | 660.1  | 978.3  | 1630.2 | 3092.8 | 4483.7  | 5773.5  | 6993.4 | 8166.4 | 9307.1 | 10424.7 | 11525,4 | 12613.3 | 136   |
|     | 5000 | 807.1  | 819.9  | 1093.4 | 1701.1 | 3125.1 | 4501.2  | 5784.5  | 7001.0 | 8172.0 | 9311.4 | 10428.2 | 11528.2 | 12615.6 | 136   |
|     | 6000 | 970.8  | 981.5  | 1220.1 | 1784.6 | 3165.5 | 4524.4  | 5799.7  | 7012.0 | B180.4 | 9318.2 | 10433.7 | 11532.9 | 12619.6 | 136   |
|     | 7000 | 1135.4 | 1144.7 | 1355.4 | 1879.1 | 3213.9 | 4553.3  | 5819.3  | 7026.4 | 8191.8 | 9327.4 | 10441.5 | 11539.6 | 12625.3 | 137   |
|     | 8000 | 1300.7 | 1308.9 | 1407 1 | 1981 1 | 1760 0 | 45,87 7 | 68411   | 7044 3 | 8706.0 | 0110 1 | 10451.4 | 11548 1 | 12632.9 | 117   |
|     |      |        |        |        |        |        |         |         |        |        |        |         |         |         |       |

#### Relationships for wellbore pressure drop as a funtion of rate using an equilibirum thermal profile

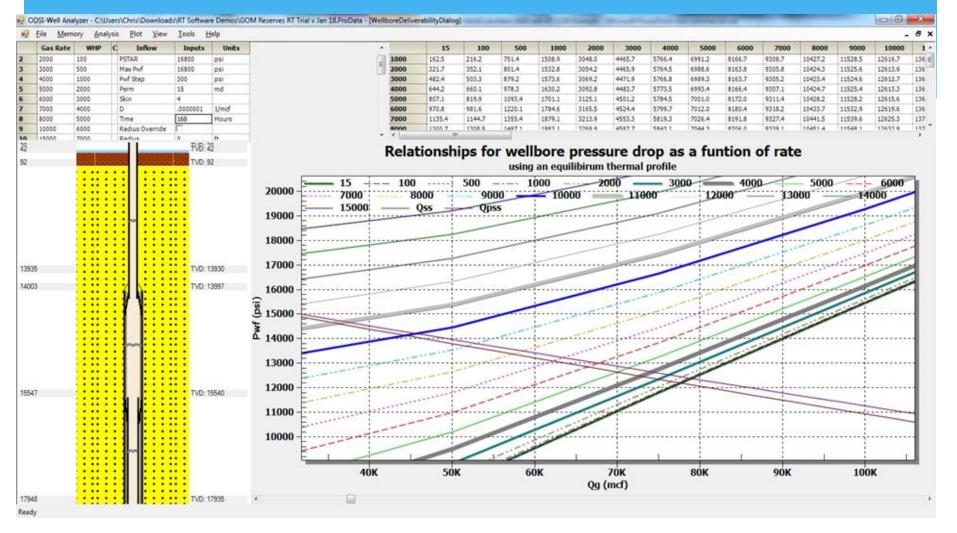


Ready

#### Inflow and VLP for Tp = 24 hours



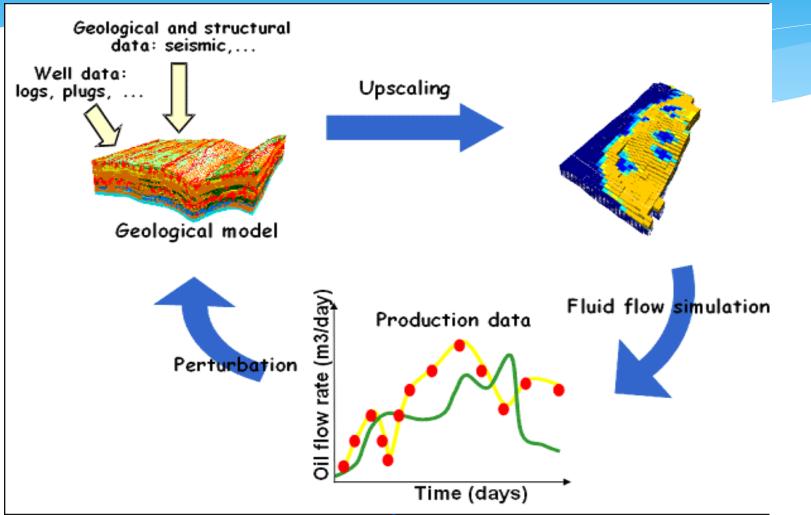
#### Inflow and VLP for Tp = 168 hours



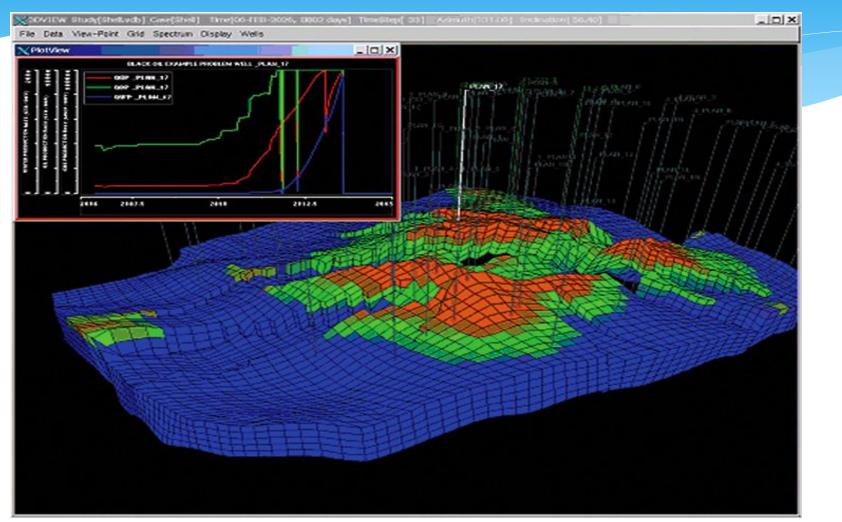
#### **Reservoir Simulation**

- Tracks behavior (esp Pressure and Saturation) in the reservoir
- \* Incorporates Multiple Wells/Multiple Zones
- Matches History and Attempts to Predict Future Performance
- \* Coupled with a Wellbore Simulator, can do amazing things
- Drawback: It takes a while to run... but they're getting faster

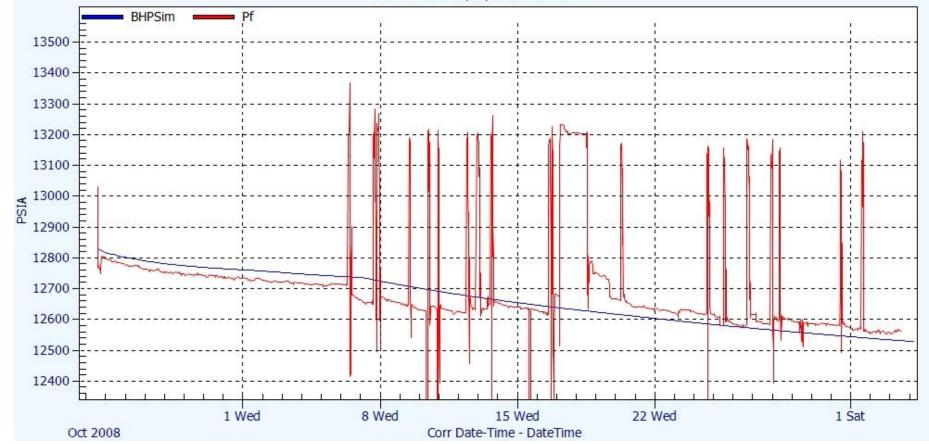
#### Simulation Gist...



#### Simulation: Well Grid



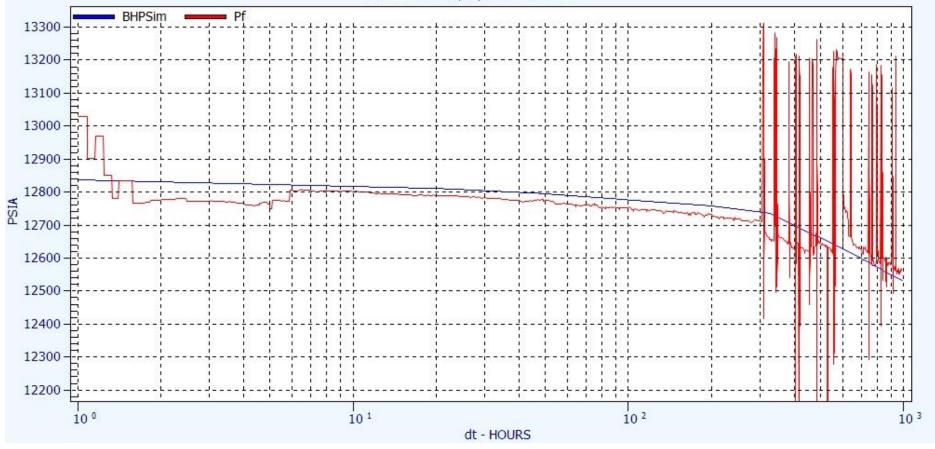
#### **Simulator Prediction vs Actual**



Date created : 8/15/2010 12:00 AM

#### Simulator Prediction vs Actual -Semilog

Date created : 8/15/2010 12:05 AM



#### Simulation Drawbacks

- Treats system as a tank model
  - \* OK for High-perm, not so good for low-perm
- \* Works best in SS or PSS flow (poor for transient)
- \* Doesn't handle discontinuities very well
- \* Subject to "gaming"
- \* Best Case Scenario: The History Match Quality is the BEST the future predictions will be...

## Components of a Real-Time Well Evaluation Package

Take all the bits and Bolt them together

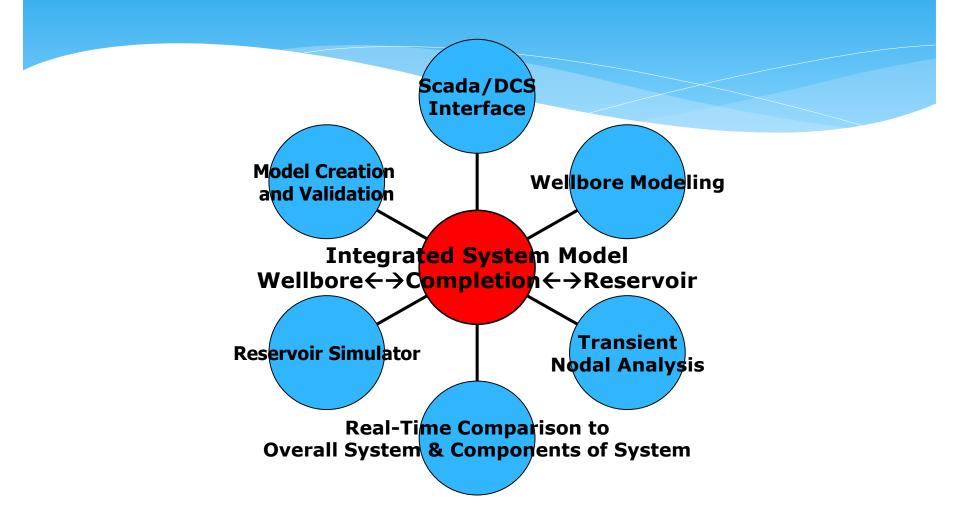
## What Do We Already Have? (Batch Process)

- \* Hopefully...adequate data frequency and quality
- \* PTA/RTA Package
- \* "Snapshot" VLP
- \* "Snapshot" Inflow
- Reservoir Simulation Tool
- \* Wellbore Model
- \* Geologic/Geo-Physical Model
- \* Enough Well History?

## What Do We Need to Make it Real-Time?

- \* Link to RT Data (w/Validation of Data)
- \* Closed-Loop Wellbore Solution (w/Thermal Modeling)
- Closed-Loop Completion Solution Can incorporate w/Reservoir Model
- \* Closed-Loop Reservoir Model
- \* Transient Recognition
- \* Boundary Recognition
- \* Regime Recognition
- \* Prediction vs. Actual Comparison
- \* Engineering by Difference (Did anything Change?)

#### ODSI Windows Service: The Bits...

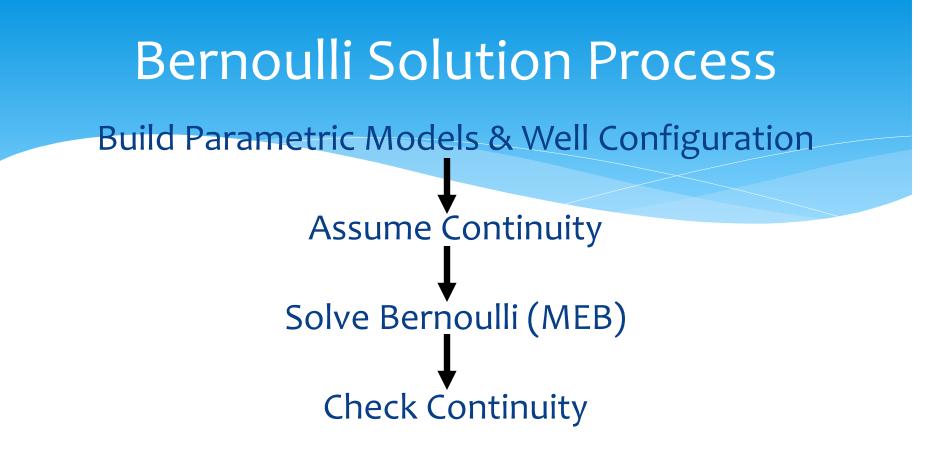


#### **Closed-Loop WB Components**

- Wellbore Thermal Modeling (Warming/Cooling)
- \* Liquid Drop Out (Build-ups)
- \* Liquid Surge (Start-up)
- \* Phase Behaviour EOS Calcs
  - \* Use SRK or PR w/Peneloux
- \* Rate Modeling
  - \* Residence Time
  - \* Rate Surging & Decay
- \* Coupled Effects (Rate-Thermal-Phase)

#### **Developing Thermal/PVT Models**

- \* Run Static Temp/Pressure Survey
- \* Run Flowing Temp/Pressure Survey
  - \* Multiple Rates
- \* Develop Heat Transfer Model Account for:
  - \* Heat Capacity of Fluids/Tubulars/Annuli/Sinks
  - \* Heat X-fer via Conduction
  - \* Heat X-fer via Convection
  - \* Heat X-fer via Forced Convection
- Can Tune PVT using same data... just get a good sample first



#### Note: If Continuity Doesn't Hold, the Well is Loading–up (which is important to know)

#### **Continuity Equation**

# $\frac{\partial \rho}{\partial t} = -(\nabla \bullet \rho v)$

 Rate of Change in Density Caused by Changes in Mass Flux

#### Differential Form of Bernoulli Eqn Compressible Conditions

 $\Delta \frac{1}{2}(v)^2 + g\Delta h + \int_{p_1}^{p_2} dp / \rho + Ws +$  $\sum_{i} \left( \frac{1}{2} v^2 \frac{L}{R_{\nu}} f \right)_i + \sum_{i} \left( \frac{1}{2} v^2 e_v \right)_i = 0$ 

#### Mechanical Energy Balance (Bernoulli Equation)

 For Single-Phase Gas Flow in Pipes, the MEB reduces to:

#### $dp/\rho = -(g \sin \theta/g_c + 2f_f u^2/g_c D) dL$

\* Basis for CS, Gray & A-C

Bernoulli for Single Phase Oil Incompressible Conditions

$$\frac{dp}{d\rho} + \frac{vdv}{g_c} + \frac{g}{g_c}dz + \frac{2f_f v^2 dL}{g_c D} + dW_s = 0$$

\* Basis for Hagedorn-Brown & Beggs/Brill

#### Simplification of Flow-in-Pipe Eqns

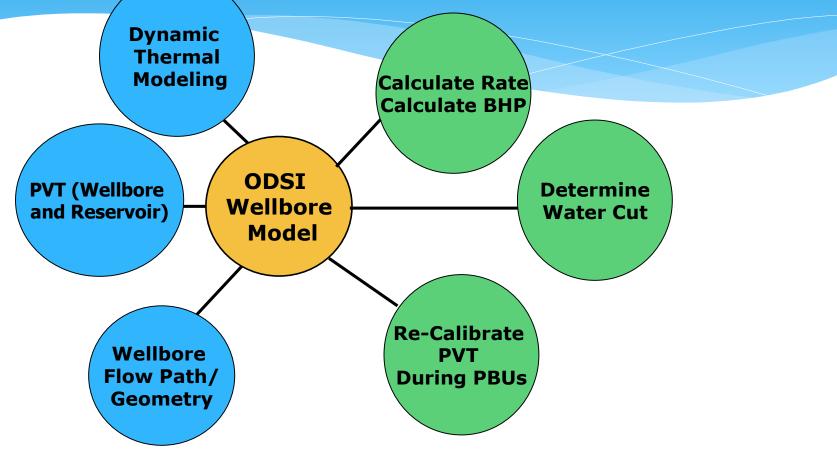
\* Conceptually, these Equations are simply:

# BHP = Gauge P + $\Delta P(\text{gravity})$ + $\Delta P(\text{friction})$

## Using a Direct Bernoulli Solution for WB

- \* Works for Oil, Gas or Water (Continuity)
- \* Gas
  - \* Have DP, solve for rate & BHP
  - \* Have Rate, solve for DP & BHP
- \* Oil
  - \* Have DP, solve for Water cut & BHP
  - \* Sometimes possible to solve for rate (high rate)
- \* Much Easier to Apply Parametric Models Continuously:
  - \* Thermal Transients
  - \* Rate Transients
  - \* Phase Transients
  - \* Coupled Rate & Thermal Transients

# What Makes ODSI's Wellbore Model Different?



#### **Completion Modeling**

- Reconcile Well Geometry (frac, horizontal, etc.) with base inflow
  - \* Multiple Layers?
  - \* Build "skin" model (easiest way if it works)
- \* Reconcile Completion/Reservoir Interaction
  - Partial Perforation/Penetration
  - \* Pay Loss/Growth
  - \* Near Well Stresses Elasto-Plastic Rock
- \* True "Afterflow" vs. Terminal Velocity Flow

#### **Closed-Loop Reservoir Solution**

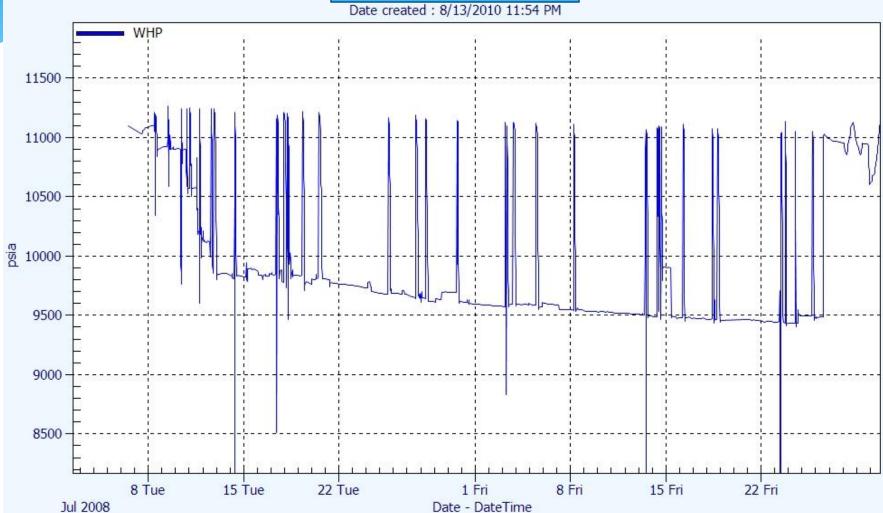
- \* Use "Static Reservoir Model" as input
- \* Use Transient Reservoir model when in transient flow
- \* Use Steady-State Reservoir model in SS flow
- \* Use Transient Recognition to "bob & weave"
- \* Objective: Run very quickly & get close
- Recognize if there's a problem with the "static" model

#### **Transient and Regime Recognition**

#### \* Locate New Transients

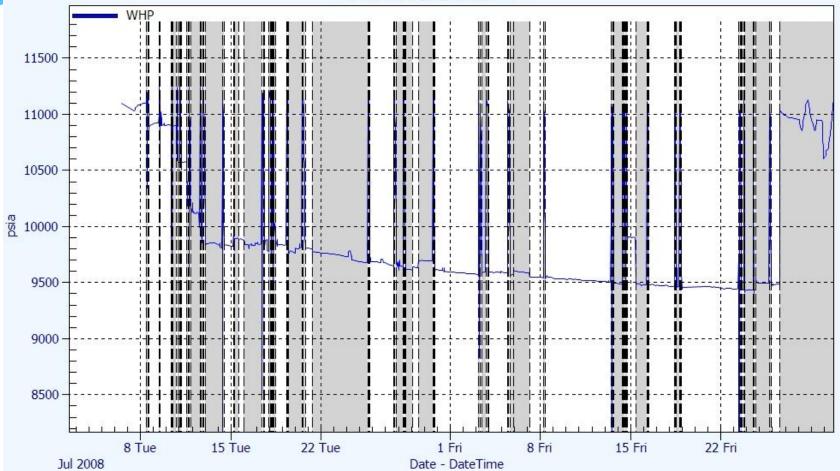
- \* Rate goes to zero, Rate stops being zero
- \* Rate changes enough to start new transient
- Pressure Methods
  - \* Wavelets
  - \* De-convolution Variance
  - \* DP Logic
- \* Banded Response Recognition
  - \* Transient vs. Steady-State
  - Boundary Recognition
  - Transition Recognition

#### **Transient Recognition**

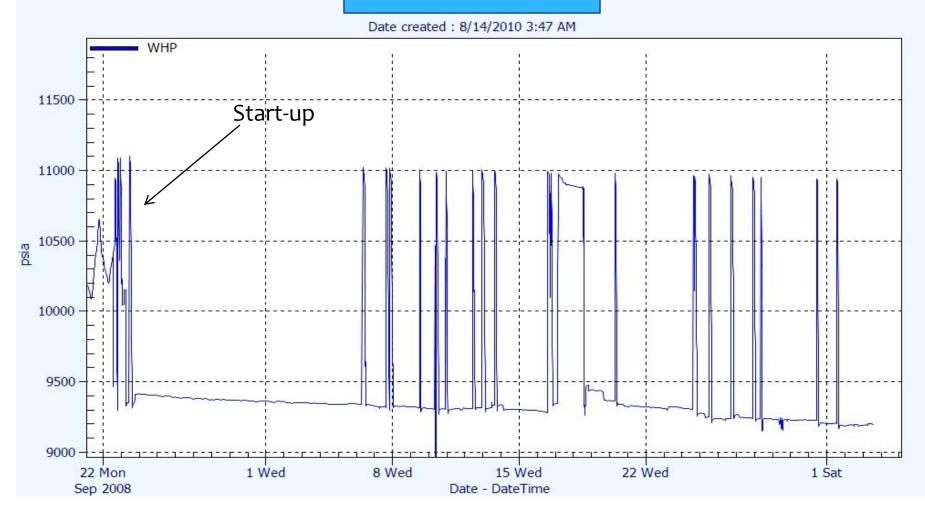


#### **Transient Recognition**

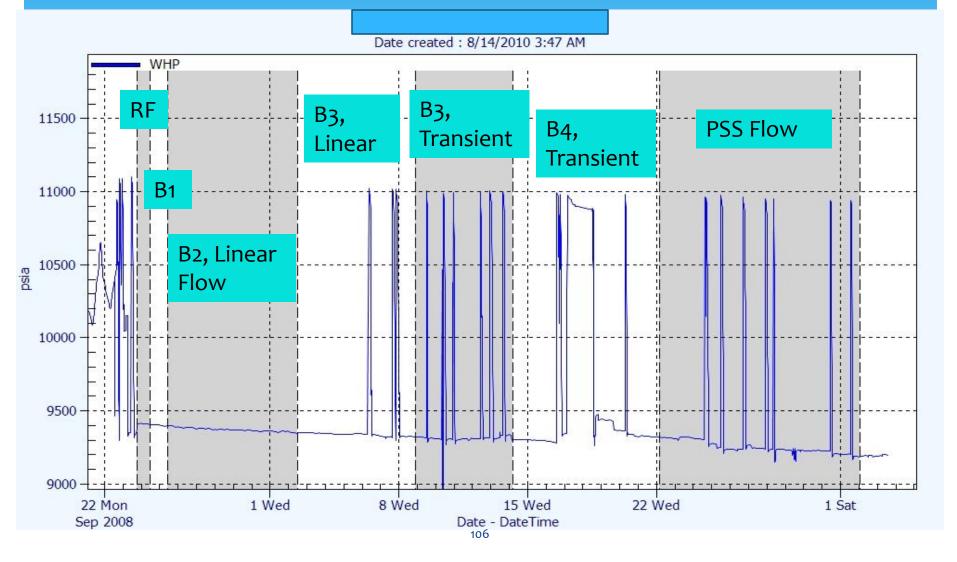
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#### **Boundary/Regime Recognition**



#### **Boundary/Regime Recognition**



# Methodology

- Start with most valid pressure measurement point
- \* Use Measured, Calculated or Inferred Rate
- Work the Mech NRG solution to WHP and mid-completion BHP
- \* Employ Complex Completion Model if Required
- \* Use Banded Energy Solution, along with Transient/Regime Recognition to determine Reservoir Inflow in both Transient and Steady-State Flow
- Bob & Weave incorporate changes in Reservoir Model as it changes (i.e. Moving Water Contact)
- \* Keep track of the important stuff & Warn PE's when something goes wrong!

#### **Translation Back to Customary Views**

- Present the Results in a way that folks are used to...
   ... or at least in terms they are accustomed to
- \* Well Test Analysis Results
- \* Productivity Tracking
- \* In-Place, Hydraulically Connected, and Mobile Hydrocarbon Volumes
- \* Reservoir Map (Energy Equivalent Map)
- \* Nodal Plots (Snapshots as function of time)
  - \* Includes Dynamic WBM & Res Inflow Model

# Strategies for Dealing with RT Data/Analysis

- Make sure that predictions match actual well behavior
- \* Look for changes!
  - \* Perm
  - \* Skin
  - \* Apparent Volumes
- \* Let the well tell you don't impose models on the well!
- \* Look for changes in the rate of change

# **Real-Time Data Strategies**

- Spend time looking for results, not just digging for data
- Validate the results; only analyze manually if you disagree... or if it's important enough to spend time on
- \* Think about what the results mean
- \* Think about how this meaning affects your decisions

If you know how much money you have left in the ground and understand the well history, you'll make better decisions

# Automated Processing Case Studies

### **Case Studies List**

- North Sea #1 Rate Calculations
- \* HPHT GOM Well Test Gas-Condy (DOT)
- \* Fizzy Oil GOM Oil well Start-up
- \* NordZee Gas Well Start-up
- \* Deepwater GOM Oil Onset of Water?
  - \* Calculated Oil-Water Splits
- \* HPHT GOM Shelf Start-up

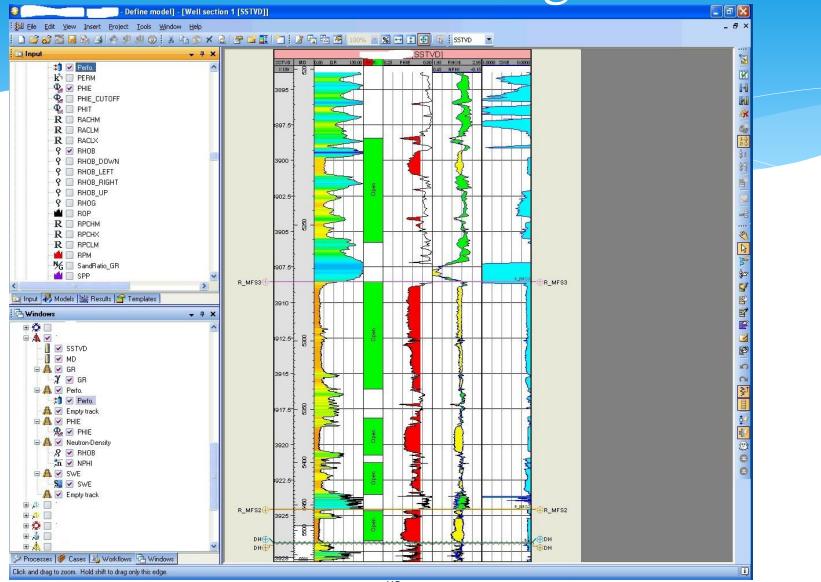
### North Sea #1 – Gas Well

- Start-up of new gas field (Subsea Trees)
- \* Well Tests have a lot of variance
- \* MDTs and PVT indicate same fluid in all zones
- \* Objectives:
  - \* Explain differences in the well test analyses
  - \* Confirm that calculated rates match measured rates

### North Sea #1 WBD

|          | : 75,4 n | n.<br>DATE : MAY/20                      |   | ANNULUS FLUID : CAC<br>INHIBITED CACL2 BRIN         |             |                    |                  |                  |            |     |
|----------|----------|--|---|---|-------------|--------------------|------------------|------------------|------------|-----|
| OMPL     | ETION    | VOLUMES                                  | 5-4-  | DRILLING DEPTHS / RT                                |             | 2                  |                  |                  |            |     |
| UBING    | VOLU     |  |   | TOL 7" LINER HANGER                                 |             | RT                 |                  |                  |            |     |
|          | /OLUM    |  |   |   |             |                    |                  |                  |            | 11  |
|          |          |  |   | TRSCSSV volume 9000-                                | ->0 psi = 1 | 00 cc              |                  | 1                |            |     |
|          |          |  | TREE 10K API / 10,000 p                         |   |             |                    |                  |                  |            | 1   |
|          | IG HEA   |  | CAMERON 4"1/16 10,0                             |   |             |                    | 0.115            |                  | liH.       |     |
|          | IG HAN   |  |   | 5" VAM TOP 13% CR W/ 3,925" S<br>API HAND GATEVALVE | RP PROF     | ILE 10,395/        | ACME             |                  |            |     |
|          | STER V   |  |   | API ACTUATOR GATEVALVE                              |             |                    |                  |                  |            |     |
|          | B VALVE  |  |   | API HAND GATEVALVE                                  | To          | bottom of it       | tem              | 1                | lil I      |     |
| FLOW     | / WING   |  | CAMERON 4"1/16 10K                              | API ACTUATOR GATEVALVE                              | length      | origin             |                  |                  | 1!         |     |
| TOP      | CAP      |  | CAMERON 6"1/2 NOM                               | INAL STUB ACME                                      | of item     | tbg. head a        |                  | Original         |            |     |
|          |          |  | STRING  |   | Length      | Depth              | ID"              | Drift SL         | li 🖂       |     |
| ITEM     | QTY      |  |   | all length to bottom                                | m.          | mTH.               | inches           | inches           | ЦЦЦ        |     |
| 1        | 1        |  | GER 13"5/8 X 4. 5" VAM T                        |   | 0.00        |                    | 3,925"           | 3,900"           | IH         |     |
| 2        | 1        |  | K-OFF STRADDLE INSTA<br>"1/2 VAM TOP 12.6# L80  |   | 1 47        | 0.00               | 2,500"<br>3,958" | 3,900"           |            | 1   |
| 2        | 1        |  | UT) 4"1/2 VAM TOP 12.6# L80                     |   | 1.47        | 2.90               | 3,958"           | 3,900"           |            | 1   |
| 4        | 1        |  | UT) 4"1/2 VAM TOP 12.6#                         |   | 2.92        | 5.82               | 3,958"           | 3,900"           |            | 1   |
|          |          |  |   |   |             | 5.82               |                  | 3,900"           |            | 1   |
| _        | 4        | TUDINOS (INCO)                           |   | 1105.0  | 10.77       | 5.82               | 0.05             | 3,900"           |            | 1   |
| 5        | 4        |  | OP 12.6# L80 13%CR (RA<br>1 TOP 12.6# L80 13%Cr | ANGE-3)   | 48.63       | 54.45<br>56.37     | 3,958"           | 3,900"<br>3.900" |            | 1   |
| 7        | 1        | Halliburton SP-1 TRS                     |   |   | 2.36        | 58.73              | 3,908            | 3,800            |            | 1   |
| 8        | 1        |  | 1 TOP 12.6# L80 13%Cr                           |   | 1.44        | 60.17              | 3,958"           | 3.833            |            | 1   |
|          |          |  |   |   |             | 60.17              |                  | Drift            | ו ור       |     |
|          |          |  |   |   |             | 60.17              |                  | Nylon            |            |     |
| 9        | 257      | TUBINGS 4"1/2 VAM T                      | OP 12.6# L80 13%CR (R/                          | ANGE-3)   | 3134.63     | 3194.80            | 3,958"           |                  |            |     |
|          |          |  |   |   |             | 3194.80<br>3194.80 |                  |                  |            |     |
|          |          |  |   |   |             | 3194.80            |                  | +                |            |     |
| 10       | 1        | PUP JOINT 4"1/2 VAM                      | TOP 12.6 # L80 13%Cr                            |   | 1.92        | 3196.72            | 3,958"           | 3.833            |            |     |
| 11       | 1        | BAKER GAUGE CARE                         |   |   | 2.29        | 3199.01            |                  | 3.833            |            |     |
| 12       | 1        |  | TOP 12.6 # L80 13%Cr                            |   | 1.44        | 3200.45            |                  | 3.833            |            |     |
| 13       | 1        |  | OP 12.6# L80 13%CR (RAM                         | NGE-3)  | 12.23       | 3212.68            |                  | 3.833            |            |     |
| 14<br>15 | 1        | PUP JOINT 4"1/2 VAM<br>HALLIBURTON 3.75" | TOP 12.6 # L80 13%Cr                            |   | 1.98        | 3214.66<br>3215.13 |                  | 3.833<br>3.833   |            |     |
| 16       | 1        |  | TOP 12.6 # L80 13%Cr                            |   | 1.46        | 3215.13            | 3,958"           | 3,833            |            | 1   |
| 17       | 1        |  | OP 12.6# L80 13%CR (RAN                         | NGE-3)  | 12.24       | 3228.83            | 3,958"           | 3.833            |            |     |
| 18       | 1        |  | TOP 12.6 # L80 13%Cr                            |   | 1.92        | 3230.75            | 3,958"           | 3.833            |            | 1   |
| 19       | 1        | HALLIBURTON PACK                         |   |   | 1.95        | 3232.70            |                  | 3.833            |            | 1   |
| 20       | 1        |  | TOP 12.6 # L80 13%Cr                            | 105.01  | 1.44        | 3234.14            |                  | 3.833            |            | 1   |
| 21       | 1        |  | DP 12.6# L80 13%CR (RAN<br>TOP 12.6 # L80 13%Cr | NGE-3)  | 12.24       | 3246.38<br>3248.30 |                  | 3.833<br>3.833   |            | 1   |
| 23       | 1        | HALLIBURTON 3.68"                        |   |   | 0.41        | 3248.71            |                  | 3.833            |            | 1   |
| 24       | 1        |  | TOP 12.6 #L80 13%Cr                             |   | 1.40        | 3250.11            |                  | 3.833            |            |     |
| 25       | 1        | PUP JOINT (SPACE-O                       | OUT) 4"1/2 VAM TOP 12.6#                        | #L80 13%Cr  | 2.95        | 3253.06            | 3,958"           | 3.833            |            | 1   |
| 26       | 1        |  | TOP 12.6 # L80 13%Cr                            |   | 1.92        | 3254.98            |                  | 3.833            |            | 1   |
| 27       | 1        | SELF ALIGNING HALF                       | MULE SHOE WIRELINE                              | IN PBR  | 2.62        | 3257.60            | 3,958"           | 3.833            |            | 1   |
|          |          |  |   | IN PBR  | 1.00        |                    |                  |                  |            |     |
|          |          |  |   |   | 1           |                    | <u> </u>         | 1                |            |     |
|          |          |  |   |   |             |                    |                  | 1                |            | - 1 |
|          |          |  |   |   |             |                    |                  |                  |            |     |
|          |          |  |   |   |             |                    |                  |                  |            |     |
| _        |          |  |   |   | +           |                    | -                | 1                |            |     |
|          |          |  |   |   | +           |                    |                  |                  |            |     |
|          |          | 1  |   |   | 1           |                    |                  | 1                |            |     |
|          |          |  |   |   |             |                    |                  | 1                |            |     |
|          |          | 3"1/2 LANDING COLLA                      | AR  |   | HUD         | 3923.30            | mTH              |                  |            |     |
| _        |          |  |   |   |             |                    |                  |                  | _ L _ L    |     |
| Perfora  | tions    |  |   |   | +           | NOT NOT            |                  |                  |            |     |
| CP       | 2" Omo   | ga poweriet 4.2 ch/8 80                  | deg. phasing 3946.0 3                           | 3982.0 mRT 36 m net.                                | -           | NOT NOR            | W CLASS          | DIFIED           |            |     |
| 91       | 2 One    | ga powerjet 4.2 st/lt 00                 | way, priability - Jerrol U J                    | www.wintti oummer.                                  | 1           | Maximum            | deviation        | 7 degrees        | @ 3390 mtr |     |
|          |          |  |   |   |             |                    |                  | . segrees        |            |     |
|          |          |  |   |   |             |                    |                  |                  |            |     |
|          |          |  |   |   |             | Rev-02             |                  |                  |            |     |
|          |          |  |   |   |             |                    |                  |                  |            |     |

### North Sea #1 Logs



### North Sea #1 - Summary

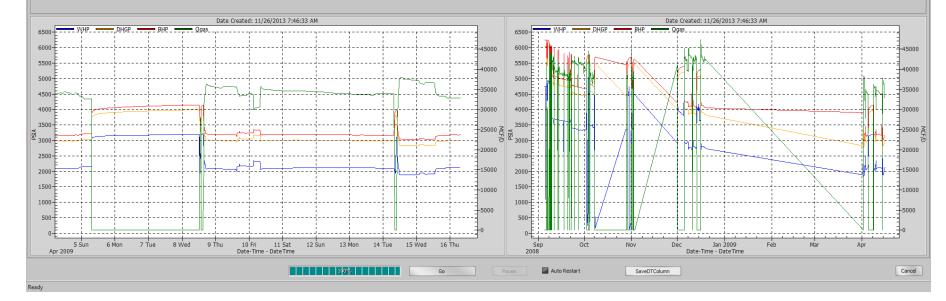
### 🏁 x64 Well Analyzer - C:\WORK\RT Software Demos\DER ver - North Sea #1 DHPG Calc Rate v Jan 18.ProData - [Real Time Testing]

🖳 File Memory Analysis Plot View Tools Help

Inputs Summary Outputs

Summary PBU DD PTA/Productivity HC Volumes P/z Derivative OilWaterRates Analysis Events

|    | Start D/T<br>ddMmmyyyy hh:mm:ss | End D/T<br>ddMmmyyyy hh:mm:ss | Test<br>Length<br>Hours | Test<br>Type | WHPi<br>psia | WHPf<br>psia | DHGPi<br>psia | DHGPf<br>psia | BHPi<br>psia | BHPf<br>psia | QGasi<br>Mcf/D | QGas<br>Mcf/D | Perm<br>md | Skin | DPskin<br>psi | PStar<br>psia | PI Eff<br>% | DPs/Q<br>psi/MMcf | Report Link           | Graph Link            |
|----|---------------------------------|-------------------------------|-------------------------|--------------|--------------|--------------|---------------|---------------|--------------|--------------|----------------|---------------|------------|------|---------------|---------------|-------------|-------------------|-----------------------|-----------------------|
| 1  | 21Sep2008 10:24:00              | 21Sep2008 14:42:00            | 4.3                     | PBU          | 3597         | 4231         | 4700          | 5266          | 4929         | 5457         | 39174          | 39174         | NaN        | NaN  | NaN           | 5848          | NaN         | NaN               | RTRep 20085ep21 10240 | RTRep 20085ep21 10240 |
| 2  | 07Oct2008 19:06:00              | 28Oct2008 21:48:00            | 506.7                   | PBU          | 3358         | 4187         | 4469          | 5120          | 4696         | 5307         | 39746          | 39746         | 9.6        | 4    | 355           | 5988          | 60          | 8.93              | RTRep 2008Oct07 19060 | RTRep 2008Oct07 19060 |
| 3  | 28Oct2008 21:48:00              | 29Oct2008 12:36:00            | 14.8                    | DD           | 4519         | 3379         | 5384          | 4457          | 5577         | 4678         | 0              | 37972         | 30.5       | 25.4 | 708           | 4627          | 20          | 18.63             | RTRep 2008Oct28 21480 | RTRep 2008Oct28 21480 |
| 4  | 29Oct2008 12:36:00              | 31Oct2008 18:36:00            | 54                      | PBU          | 3386         | 389          | 4457          | 5504          | 4678         | 5701         | 37833          | 37833         | 9.6        | 4    | 339           | 5701          | 60          | 8.95              | RTRep 20080ct29 12360 | RTRep 2008Oct29 12360 |
| 5  | 01Dec2008 07:00:00              | 05Dec2008 09:54:00            | 98.9                    | PBU          | 2912         | 3535         | 3992          | 4621          | 4217         | 4795         | 41009          | 41009         | 8.2        | 2.5  | 269           | 5584          | 70          | 6.55              | RTRep 2008Dec01 07000 | RTRep 2008Dec01 07000 |
| 6  | 05Dec2008 09:54:00              | 10Dec2008 15:48:00            | 125.9                   | DD           | 4190         | 2757         | 5199          | 3857          | 5388         | 4085         | 0              | 43293         | 37.4       | 34.2 | 905           | 3376          | 16          | 20.91             | RTRep 2008Dec05 09540 | RTRep 2008Dec05 09540 |
| 7  | 11Dec2008 05:42:00              | 13Dec2008 16:24:00            | 58.7                    | DD           | 4776         | 2843         | 5044          | 3899          | 5229         | 4126         | 0              | 42717         | 13.2       | 7.7  | 571           | 3824          | 44          | 13.38             | RTRep 2008Dec11 05420 | RTRep 2008Dec11 05420 |
| 8  | 13Dec2008 17:48:00              | 16Dec2008 11:00:00            | 65.2                    | PBU          | 2742         | 4139         | 3844          | 5102          | 4074         | 5289         | 42749          | 42749         | 9.7        | 4.5  | 439           | 5489          | 57          | 10.26             | RTRep 2008Dec13 17480 | RTRep 2008Dec13 17480 |
| 9  | 16Dec2008 11:00:00              | 20Dec2008 06:00:00            | 91                      | DD           | 3806         | 2728         | 5102          | 3814          | 5289         | 4041         | 0              | 43577         | 12         | 6.5  | 546           | 3723          | 48          | 12.52             | RTRep 2008Dec16 11000 | RTRep 2008Dec16 11000 |
| 10 | 05Apr2009 07:12:00              | 08Apr2009 12:48:00            | 77.6                    | PBU          | 2167         | 2853         | 3025          | 3654          | 3207         | 3799         | 32625          | 32625         | 9.7        | 3.6  | 283           | 4346          | 62          | 8.66              | RTRep 2009Apr05 07120 | RTRep 2009Apr05 07120 |



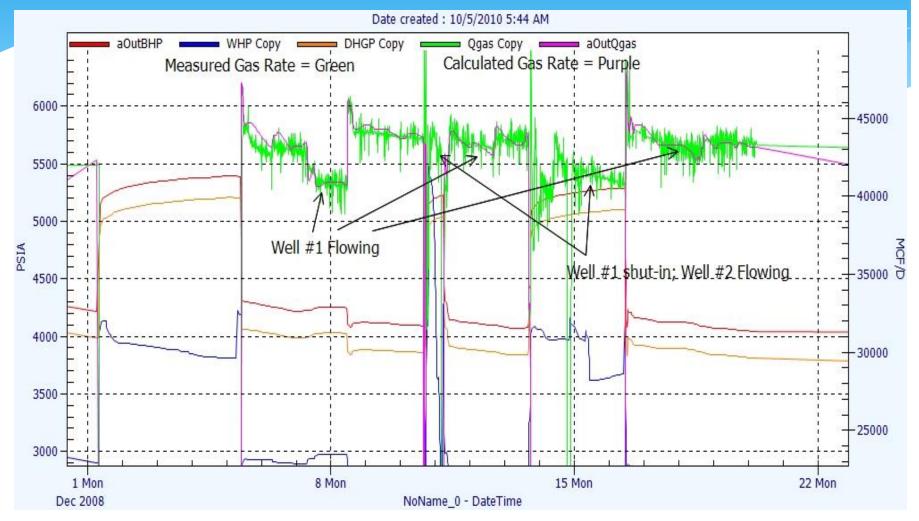
### North Sea #1 - PBUs

| U DD PTA/ Produ                            | ctivity HC Volumes P/z |                         | /e OilWate   | rRates Ana                            | alysis Events |               |               |              |              |                |               |   |   |               |               |             |                  |                                       |  |  |
|--|------------------------|-------------------------|--------------|---------------------------------------|---------------|---------------|---------------|--------------|--------------|----------------|---------------|---|---|---------------|---------------|-------------|------------------|---------------------------------------|--|--|
| Start D/T<br>Immyyyy hh:mm:ss dd           |                        | Test<br>Length<br>Hours | Test<br>Type | WHPi<br>psia                          | WHPf<br>psia  | DHGPi<br>psia | DHGPf<br>psia | BHPi<br>psia | BHPf<br>psia | QGasi<br>Mcf/D | QGas<br>Mcf/D | Perm 5  | ikin  | DPskin<br>psi | PStar<br>psia | PI Eff<br>% | DPs/Q<br>psi/MMc | f Report Link                         | Graph Link   |  |
| ep2008-10:24:00 2:                         |                        | 4.3                     | PBU          | 3597                                  | 4231          | 4700          | 5266          | 4929         |              |                |               |   | NaN   | NaN           | 5848          | NaN         |                  |                                       | 40 RTRep 20085ep21 10240                                   |  |
| ct2008 19:06:00 28                         |                        | 506.7                   | PBU          | 3358                                  | 4187          | 4469          | 5120          | 4696         |              | 39746          |               | 9.6   | 4   | 355           | 5988          | 60          |                  | RTRep 20080ct07 1906                  | O LIC DDILing  |  |
| Oct2008 12:36:00 3:<br>Dec2008 07:00:00 05 |                        | 54<br>98.9              | PBU<br>PBU   | 3386<br>2912                          | 389<br>3535   | 4457<br>3992  | 5504<br>4621  | 4678<br>4217 |              | 37833<br>41009 |               | 9.6<br>8.2  | 4<br>2.5  | 339<br>269    | 5701<br>5584  | 60<br>70    |                  | 5 RTRep 2008Oct29 1236                | 0 115 DPU inc<br>0 115 DPU inc<br>00 RTRep 2008Dec01 07000 |  |
| Dec2008 17:48:00 16                        |                        | 65.2                    | PBU          | 2742                                  | 4139          | 3844          | 51021         | 4074         |              | 42749          |               | 9.7   | 4.5   | 439           | 5489          |             |                  | 5 RTRep 2008Dec13 1748                | 80 RTRep 2008Dec13 17480                                   |  |
| 5Apr2009 07:12:00 08                       |                        | 77.6                    | PBU          | 2167                                  | 2853          | 3025          | 3654          | 3207         | 3799         | 32625          | 32625         | 9.7   | 3.6   | 283           | 4346          | 62          |                  |                                       | 20 RTRep 2009Apr05 07120                                   |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               |   |   |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               |   |   |               |               |             |                  |                                       |  |  |
| WHP DHGP                                   | ВНР                    | Dat<br><u>Ogas</u>      | te Created   | : 11/26/20:                           | 13 7:46:33    | AM            |               |              |              |                |               |   |   |               | Out BHP       |             | M1(v=00.)        |                                       | /26/2013 7:46:14 AM<br>P1(y=146.8*log(x)+3870)             |  |
|  |                        | 2900                    |              |                                       |               |               |               |              |              |                |               |   | t:  | 1.1           | out bill      |             | 10 700           |                                       |  |  |
|  |                        |                         |              |                                       | ļ             |               |               |              |              |                |               | 45000   | 4100-   |               |               |             |                  | · · · · · · · · · · · · · · · · · · · |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               | 45000   | 4100-   |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               |   | 4100  |               |               |             |                  |                                       |  |  |
|  |                        |                         |              | · · · · · · · · · · · · · · · · · · · |               | ·             |               | +-           |              | ~              |               | 40000   | 4000  |               |               |             |                  | · · · · · · · · · · · · · · · · · · · |  |  |
| ~~~  |                        |                         |              |                                       |               |               |               |              |              | <u> </u>       |               | 40000   | Ī   |               |               |             |                  |                                       |  |  |
| ~  |                        |                         |              |                                       |               |               |               |              |              | ·              |               | 40000   | 4000  |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              | <u> </u>       |               | 40000<br>35000<br>30000                                 | 4000  |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               | 40000<br>35000<br>30000<br>-25000 MCF                   | 4000<br>3900<br>3800<br>3800<br>3700<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4 |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              | <u>``</u>      |               | 40000<br>35000<br>30000<br>-25000 MCF                   | 4000<br>3900<br>3800  |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               | 40000<br>35000<br>30000<br>25000 MGP<br>50<br>220000    | 4000<br>3900<br>3800<br>3800<br>3700<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4<br>4 |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              | <u> </u>       |               | 40000<br>35000<br>30000<br>225000 Mg<br>20000<br>15000  | 4000<br>3900<br>3800<br>3700<br>3600<br>3500  |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               | 40000<br>35000<br>30000<br>225000 Mg<br>20000<br>15000  | 4000<br>3900<br>3800<br>3700  |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               | 40000<br>35000<br>225000 M K<br>20000<br>15000<br>10000 | 4000<br>3900<br>3800<br>3700<br>3600<br>3500  |               | /             |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               | 40000<br>35000<br>25000 K<br>20000<br>15000<br>10000    | 4000<br>3900<br>3800<br>3700<br>33500<br>33500  |               |               |             |                  |                                       |  |  |
|  |                        |                         |              |                                       |               |               |               |              |              |                |               | 40000<br>35000<br>22000 AG<br>22000<br>10000<br>5000    | 4000<br>3900<br>3800<br>3700<br>33500<br>33500  |               |               |             |                  |                                       |  |  |

### North Sea #1 - DDs

| ary Outpu            | nalysis <u>P</u> lot <u>V</u> i<br>15 |                           |                         |              |               |                      |         |              |              |                       |            |  |               |               |             |                   |                       |                                      |
|----------------------|---------------------------------------|---------------------------|-------------------------|--------------|---------------|----------------------|---------|--------------|--------------|-----------------------|------------|--|---------------|---------------|-------------|-------------------|-----------------------|--------------------------------------|
| DD                   | PTA/ Productivity                     | HC Volumes P/z            | Deriva                  | tive OilWate | erRates Analy | sis Events           |         |              |              |                       |            |  |               |               |             |                   |                       |                                      |
| Start D/<br>myyyy hi | r<br>:mm:ss ddMmn                     | End D/T<br>ayyyy hh:mm:ss | Test<br>Length<br>Hours | Test<br>Type |               | 'HPf DHG<br>sia psia |         | BHPi<br>psia | BHPf<br>psia | QGasi QG<br>Mcf/D Mcf | Perm<br>md | Skin   | DPskin<br>psi | PStar<br>psia | PI Eff<br>% | DPs/Q<br>psi/MMcf | Report Link           | Graph Link                           |
| :t2008-2             | 1:48:00 29Oct                         | 2008 12:36:00             | 14.8                    | DD           | 4519          | 3379 53              | 84 4457 | 5577         | 4678         | 0 379                 | 2 30.5     | 25.4   | 708           | 4627          | 20          | 18.63             | RTRep 2008Oct28 21480 | 0 RTRep 2008Oct28 21480              |
| 2008 Oʻ              | 9:54:00 10Dec                         | 2008 15:48:00             | 125.9                   | DD           | 4190          | 2757 5:              | 99 3857 | 5388         | 4085         | 0 432                 | 3 37.4     | 34.2   | 905           | 3376          |             |                   | RTRep 2008Dec05 0954  | 0 RTRep 2008Dec05 09540              |
| 2008-0               | 5:42:00 13Dec                         | 2008 16:24:00             | 58.7                    | DD           | 4776          | 2843 50              | 44 3899 | 5229         | 4126         | 0 427                 | 7 13.2     | 7.7  | 571           | 3824          |             |                   |                       | 0 UC DD ing                          |
| 2008 1               | 1:00:00 20Dec                         | 2008 06:00:00             | 91                      | DD           | 3806          | 2728 5:              | 02 3814 | 5289         | 4041         | 0 435                 | 7 12       | 6.5  | 546           | 3723          | 48          | 12.52             | RTRep 2008Dec16 11000 | 0 RTRep 2008Dec16 11000              |
|                      |                                       |                           |                         |              |               |                      |         |              |              |                       |            |  |               |               |             |                   |                       |                                      |
| ľ                    |                                       |                           | D                       | ate Created  | : 11/26/2013  | 7:46:33 AM           |         |              |              |                       |            |  |               |               |             |                   | Date Created: 11/     | 26/2013 7:46:14 AM                   |
| -                    | DHGP -                                | BHP                       | Qgas                    |              |               |                      |         |              |              |                       |            |  |               |               |             | M1/v=00.0         | *la e(u) - 2040 4)    | D4(- 445 08(-)-0070)                 |
| Ψ <u>Η</u> Ρ         |                                       |                           |                         |              |               |                      |         |              |              |                       |            |  | 2 3 3         | Out BHP       | ·           | M1(x-90.0         | *log(x)+3948.4)       | P1(y=146.8*log(x)+3870)              |
|                      |                                       |                           |                         |              |               |                      |         |              |              |                       |            | 4100-  |               | Out BH        |             |                   |                       | P1(y=146.8 <sup>-10</sup> g(x)+3870) |
| -+                   |                                       |                           |                         | <br>         |               |                      |         | +-           |              | ~                     |            | 4100-<br>4000-<br>3900-  |               | Out BH        |             |                   |                       | ·                                    |
|                      |                                       |                           |                         | <br><br>     |               |                      |         |              |              | <u></u>               |            | 4000-  |               | Out BH        |             |                   |                       |                                      |
|                      |                                       |                           |                         |              |               |                      |         |              |              |                       |            | 4000-<br>3900-<br>3800-<br>3800-<br>3700-                        |               | Out BH        |             |                   |                       |                                      |
|                      |                                       |                           |                         |              |               |                      |         |              |              |                       |            | 4000-<br>3900-<br>3800-<br>3800-                                 |               | Out BH        |             |                   |                       |                                      |
|                      |                                       |                           |                         |              |               |                      |         |              |              |                       |            | 4000-<br>3900-<br>3800-<br>3800-<br>3700-<br>3600-               |               |               |             |                   |                       |                                      |
|                      |                                       |                           |                         |              | <br>          |                      |         |              |              |                       |            | 4000-<br>3900-<br>3800-<br>3800-<br>X<br>3700-<br>3500-<br>3500- |               | Out BH        |             |                   |                       |                                      |
|                      |                                       |                           |                         |              |               |                      |         |              |              |                       |            | 4000-<br>3900-<br>3800-<br>3700-<br>3600-<br>3500-<br>3400-      |               | Out BH        |             |                   |                       |                                      |

# North Sea #1 Rate Check



### North Sea #1 - Conclusions

- \* Rates (measured vs. calculated) appear valid
- \* Build-ups are consistent perm of 10md, skin of 3-ish
- \* Drawdowns are all over the place
  - Maybe related to zonal flow?
  - No consistent explanation
- Ignore DD's use PBUs for evaluations of change

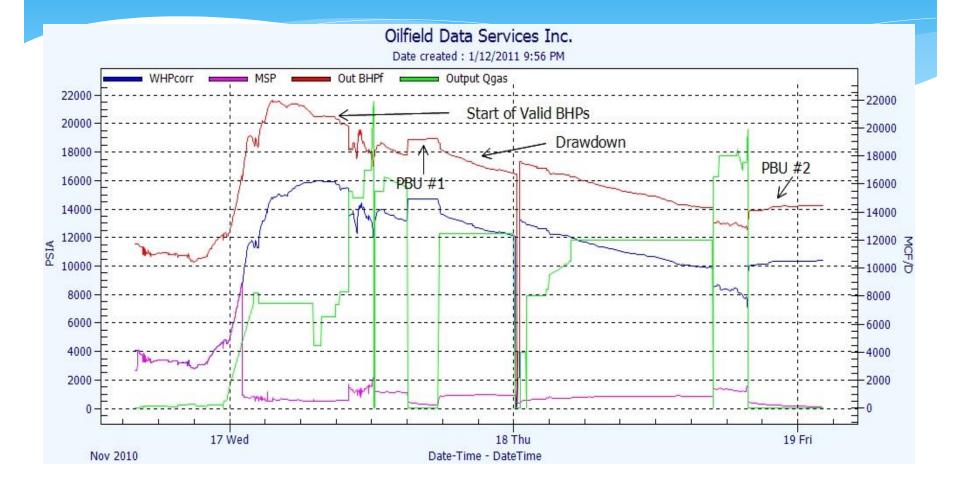
# HPHT GOM Gas-Condy Extended Well Test

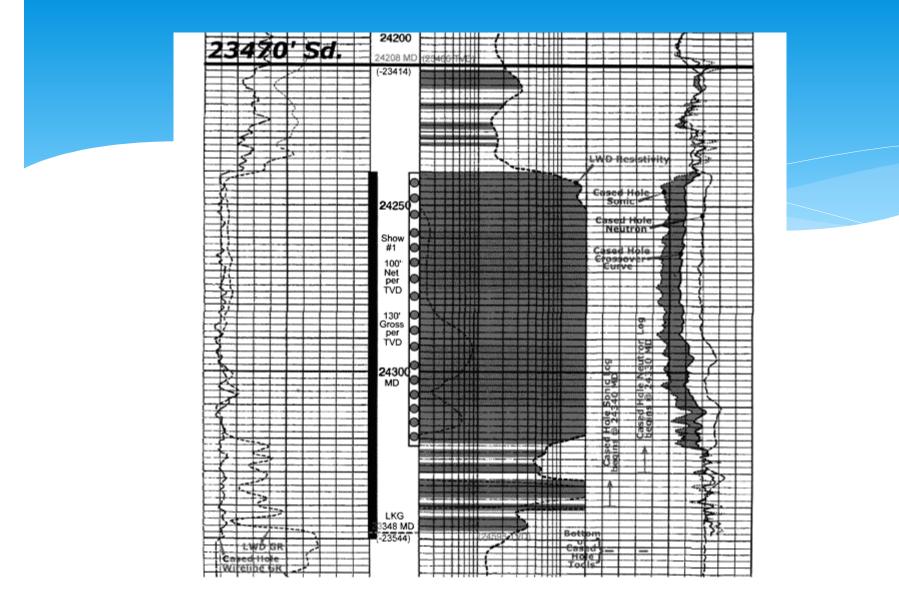
### Set-up:

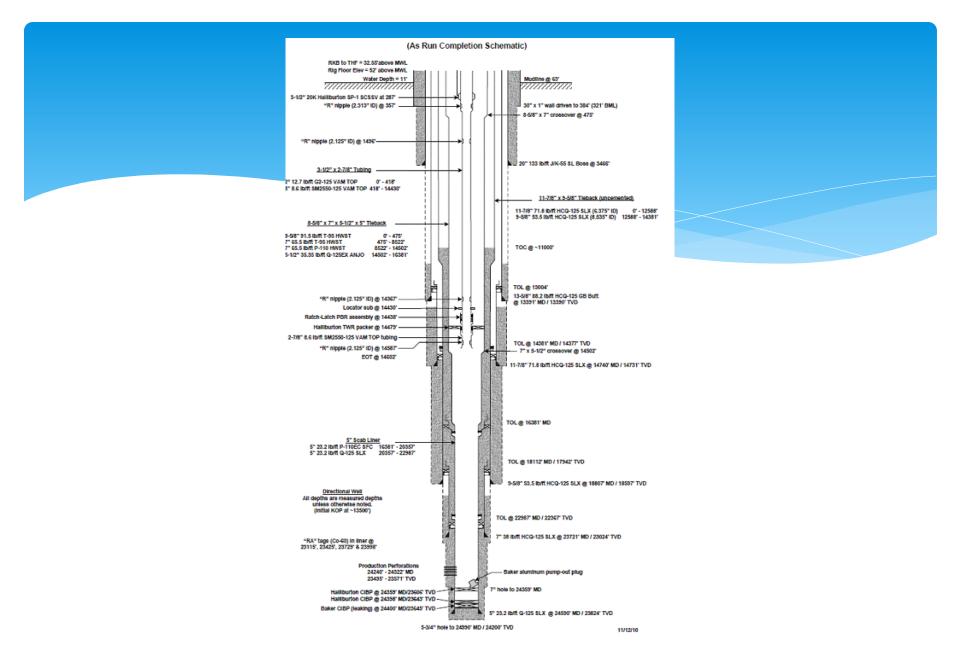
- \* Well Flowed-Back 6 months before
- "Discredited" Well Test/Reservoir Engineer said it Depleted on Test
- \* Supposed to be upwards of 1 TCF of reserves in field
- \* Temporary MOPU on location
- \* Rock Could Be 'Squishy'
- \* Good CBL
- \* Packer could be a weak point

Objective: Determine if reserves justify a platform

## Whaddaya Think?







### **DOT - Summary**

### 🕨 x64 Well Analyzer - C:\WORK\RT Software Demos\DOT #1 - UHPHT GOM using outBHP.ProData - [Real Time Testing] - 🖬 🗙 Pile Memory Analysis Plot View Tools Help Inputs Summary Outputs Summary PBU DD PTA/ Productivity HC Volumes P/z Derivative OilWaterRates Analysis Events Test End D/T QGas PStar DPs/Q Shart D/T Tesl WHP WHD DHGPi DHGPf BHP BHP QGas DPskin PI Eff Length Skin Report Link Graph Link ddMmmyyyy hh:mm:ss ddMmmyyyy hh:mm:ss Туре psia Mcf/D Mcf/D md psia 06 psi/MMcf psia psia psia osia psia DSİ Hours 309 -388.0 RTRep 2011May04 1016 RTRep 2011May04 1016 1 04May2011 10:16:19 04May2011 19:20:04 9.06 DD 14286 8946 -1 -1 18619 13553 0 13298 0.2 -2.4 -5161 9100 PBU 7 174.2 RTRep 2011May04 1923 RTRep 2011May04 1923 04May2011 19:23:04 04May2011 20:23:49 1.01 9188 12061 13734 16149 14607 14607 70.5 2545 16540 2 -1 -1 11.3 149 -163.8 RTRep 2011May04 2141 RTRep 2011May04 2141 3 04May2011 21:41:04 05May2011 18:29:49 20.81 DD 13972 7734 -1 -1 17918 11482 0 14118 0.2 -1.2 -2314 9402 16 96.14 RTRep 2011May05 1830 RTRep 2011May05 1830 05May2011 18:30:04 12May2011 04:55:10 154.42 PBU 7182 3363 -1 -1 11067 6076 8016 8016 7.3 27.2 771 12629 4 12May2011 04:55:10 13May2011 03:06:25 22.19 DD 3385 5708 6107 9234 0 4870 -3.8 -2276 8117 399 -4675. RTRep 2011May12 0455 RTRep 2011May12 0455 5 -1 -1 0 13May2011 03:06:25 13May2011 16:27:40 PBU 5746 6869 -1 9279 10428 5705 5705 NaN NaN NaN 63218 NaN NaN RTRep 2011May13 0306 RTRep 2011May13 030 RTRep 2011May13 1627 13May2011 16:27:40 17May2011 06:05:55 85.64 DD 6941 2939 -1 -1 10511 5555 0 8000 0 -2.8 -1285 5715 33258 -1606. RTRep 2011May13 1627 RTRep 2011May17 0607 RTRep 2011May17 0607 8 17May2011 06:07:25 17May2011 13:03:40 6.94 PBU 2900 3587 -1 -1 5499 6339 3606 3606 0.8 1.3 140 6754 76 38.91 323 -451.0 RTRep 2011May17 1303 RTRep 2011May17 1303 17May2011 13:03:40 18May2011 04:07:10 9 15.06 DD 3582 2652 -1 -1 6332 5153 0 3250 0.1 -2.1 -1466 4778 18May2011 17:02:10 18May2011 21:01:25 3.99 PBU 2502 3064 -1 4912 5615 **3005** 3005 0.4 -0.5 -89 5983 116 -29.59 RTRep 2011May18 1702 RTRep 2011May18 1702 10 -1 Date Created: 11/26/2013 8:06:38 AM Date Created: 11/26/2013 8:06:38 AM BHP BHP Qgas Qgas -16000 -16000 18000 18000 -14000 -14000 16000 16000 --12000 12000 14000 14000--10000 -10000 12000 12000-¥ 10000 8000 MCF 10000--8000 ਨੂੰ 8000 8000 -6000 -6000 6000 6000 4000 4000 4000 4000 -2000 -2000 2000 2000 6PM 18 Wed 3AM 6AM 9ÅM 12PM 3PM 6PM 9PM 8 Sun 15 Sun 3DM 9PM 17 Tue May 2011 Date-Time - DateTime May 2011 Date-Time - DateTime 100% Cancel Go Auto Restart SaveDTColumn 125

### DOT - PBUs

|                  | Memory Analysis I               | Plot View Tools Help          | )                       |              |                    |                |               |   |              |              |                |               |            |       |             |               |                  |                  |               |                           |                          |  |
|------------------|---------------------------------|-------------------------------|-------------------------|--------------|--------------------|----------------|---------------|---|--------------|--------------|----------------|---------------|------------|-------|-------------|---------------|------------------|------------------|---------------|---------------------------|--------------------------|--|
|                  | Summary Outputs                 |                               |                         |              |                    |                |               |   |              |              |                |               |            |       |             |               |                  |                  |               |                           |                          |  |
| er'              | PBU DD PTA/P                    | roductivity HC Volumes P/z    | Derivat                 | ive OilWat   | erRates Ar         | nalysis Events | •]            |   |              |              |                |               |            |       |             |               |                  |                  |               |                           |                          |  |
|                  | Start D/T<br>ddMmmyyyy hh:mm:ss | End D/T<br>ddMmmyyyy hh:mm:ss | Test<br>Length<br>Hours | Test<br>Type | WHPi<br>psia       | WHPf<br>psia   | DHGPi<br>psia | DHGPf<br>psia                             | BHPi<br>psia | BHPf<br>psia | QGasi<br>Mcf/D | QGas<br>Mcf/D | Perm<br>md | Skin  |             | PStar<br>psia | PI Eff I<br>% ps | DPs/Q<br>ii/MMcf | Report Link   |                           | Graph Link               |  |
| t                | 04May2011 19:23:04              | 04May2011 20:23:49            | 1.01                    | PBU          | 9188               | 12061          | -1            | -1  | 13734        | 16149        | 14607          | 14607         | 11.3       | 70.5  | 2545 1      | 6540          | 7                | 174.2            | TRep 2011May0 | 4 1923                    | RTRep 2011May04 1923     |  |
|                  |                                 | 12May2011 04:55:10            |                         | PBU          | 7182               | 3363           | -1            |   | 11067        | 6076         |                | 8016          |            | 27.2  | 771 1       |               |                  |                  | TRep 2011May0 | 5 1830                    | RTRep 2011May05 1830     |  |
|                  |                                 | 17May2011 13:03:40            | 6.94                    | PBU          | 2900               | 3587           | -1            | -1  | 5499         | 6339         | 3606           | 3606          | 0.8        | 1.3   | 140         | 6754          | 76 3             | 38.91            | TRep 2011May1 | 7 0607                    | RTRep 2011May17 0607     |  |
|                  | 18May2011 17:02:10              | 18May2011 21:01:25            | 3.99                    | PBU          | 2502               | 3064           | -1            | -1  | 4912         | 5615         | 3005           | 3005          | 0.4        | -0.5  | -89         | 5983          | 116 -:           | 29.59            | TRep 2011May1 | 8 1702                    | RTRep 2011May18 1702     |  |
|                  |                                 |                               |                         |              |                    |                |               |   |              |              |                |               |            |       |             |               |                  |                  |               |                           |                          |  |
|                  |                                 |                               | D;                      | ate Creater  | 1: 11/26/20        | 013 8:06:38    | AM            |   |              |              |                |               |            |       |             |               |                  |                  | Date Create   | ed: 11/26/                | 2013 8:06:38 AM          |  |
|                  | WHP                             | BHP Qgas                      |                         | 1            | 1                  | 1              |               | 1   |              |              | 1              |               | 16000      |       |             | Out BHP       | M1               | (y=196.4*        |               |                           | L(y=268.2*log(x)+5446.2) |  |
|                  |                                 |                               |                         | 1            |                    |                |               |   |              |              | 1              |               |            | 5600- |             |               |                  |                  |               | 1 1 1<br>1 1 1<br>+ -   - |                          |  |
| 01               |                                 |                               |                         |              |                    | ····           |               |   |              |              | +              |               |            | 5000  | - i - i - i |               |                  |                  |               |                           |                          |  |
|                  |                                 |                               |                         |              |                    |                |               |   |              |              | -              | 1             | 14000      | E     | 1 1 1       | 1111          |                  |                  |               |                           |                          |  |
| 0                | - -                             | ·l                            |                         | L            |                    | ·····          |               |   |              |              | +              | ·             |            | 5500- | 1 1 1       |               |                  | 44               |               | 1 1 1                     |                          |  |
|                  | t i                             |                               |                         | 1            |                    |                |               |   |              |              | 1              | 1             | 12000      | Ę     |             |               |                  |                  |               |                           |                          |  |
| 00               |                                 |                               |                         | ;            |                    |                |               |   |              |              | ÷              | ·             |            | 5400- |             |               |                  |                  |               | +                         |                          |  |
|                  |                                 |                               |                         | <br> <br>    |                    |                |               |   |              |              | 1              |               |            | F     |             |               |                  |                  |               |                           |                          |  |
| )                |                                 |                               |                         | +<br>¦       | !                  | ·              |               | -+  |              |              | +              |               | 10000      | FROM  |             |               |                  |                  |               |                           |                          |  |
|                  | E                               |                               |                         | 1            |                    |                |               | Ì   |              |              | į              |               |            | 5300- |             |               |                  |                  |               | 世                         |                          |  |
| )                |                                 |                               |                         | ¦            |                    | ····           |               |   |              |              | +              |               | 8000 MCF/D | K -   | i i i       |               |                  |                  |               | M                         |                          |  |
|                  | H i                             |                               |                         |              |                    |                |               |   |              |              | 1              | 1             | 9 g        | 5200- |             |               |                  | ++               |               | +                         | /                        |  |
|                  |                                 |                               |                         |              |                    | ····           |               |   |              |              | <u>+</u>       |               | 6000       | E     |             |               |                  |                  |               |                           |                          |  |
| 00               | Fi i i                          |                               |                         |              |                    |                |               |   |              |              | 1              | 1             | 0000       | 5100- |             |               |                  |                  |               | <u>7</u> 0                |                          |  |
|                  | - I I                           |                               |                         | <u>ہ</u>     |                    | ·              |               |   |              |              | +              |               |            | 5100- | iii         | 1111          |                  |                  |               | 111                       |                          |  |
|                  |                                 |                               |                         |              |                    |                |               |   |              | _(           | 1              | 1             | 4000       | E     |             |               |                  |                  |               |                           |                          |  |
| 00               |                                 |                               |                         |              |                    |                |               | <u></u>                                   |              |              | +              |               |            | 5000- |             |               |                  | +                | •             | +                         |                          |  |
| 01               |                                 |                               |                         |              |                    |                |               | 1   |              | -            |                | ; 1           | 2000       | E     |             |               |                  |                  |               |                           |                          |  |
| 101              |                                 |                               |                         |              |                    |                |               |   |              |              | +              |               |            | 4900- |             |               |                  | 1 İ              | - i i i i     | i i i                     | i i i                    |  |
| 01               |                                 |                               |                         |              |                    |                |               |   |              |              | į.             | 1             |            |       |             |               |                  |                  |               | 4-1-1                     |                          |  |
|                  |                                 |                               |                         |              |                    |                |               |   |              |              |                |               |            | 4900- |             |               |                  | ·                |               | +                         |                          |  |
| )                |                                 |                               |                         |              |                    |                |               | -+<br> <br> <br> <br> <br> <br> <br> <br> |              |              |                |               | 0          | 4900- |             |               |                  | ·                |               | +                         |                          |  |
| 01               | 3PM 6PM                         | 9PM 18 Wed                    | 3/                      |              | 6AM                |                |               | <br><br>12PM                              | 3PM          | 6            | <br>           | 9PM           | 0          | 4900  |             |               | -2               |                  |               | 10-1                      |                          |  |
| )<br>)<br>)<br>) |                                 | 9PM 18 Wed                    | 3/                      |              | 6AM<br>e-Time - Da |                |               | 12PM                                      | ЗРМ          | 6            | РМ             | 9PM           | 0          | 4900- |             |               | -2               |                  |               | 10-1                      | t: May-18-2011 17:02:10] |  |

Ready

# DOT - Productivity

| 4 Well Analyzer - C:\WORK\RT Software Demos\                            |                   | using outBHP.ProData - [Real Time Testing | g]     |       |                   |          |                                     |     |
|---|-------------------|---|--------|-------|-------------------|----------|-------------------------------------|-----|
| <u>File M</u> emory <u>A</u> nalysis <u>P</u> lot <u>V</u> iew <u>T</u> | ools <u>H</u> elp |   |        |       |                   |          |                                     |     |
| ts Summary Outputs  | human D/a Daniur  |   |        |       |                   |          |                                     |     |
| itial Pres (PSIA)   | O O               | tive OilWaterRates Analysis Events        |        |       |                   |          |                                     |     |
| ist PBU DPskin/Q (PSI/(MMCF/D))   | -29.59            | 05/18/2011 21:01:25                       |        |       |                   |          |                                     |     |
| ist DD DPskin/Q (PSI/(MMCF/D))  | -451.07           | 05/18/2011 04:07:10                       |        |       |                   |          |                                     |     |
| st P* (PSIA)  | 5983              | 05/18/2011 21:01:25                       |        |       |                   |          |                                     |     |
| st Productivity Q/DP (MCF/D/PSI)  | 0.166             | 05/18/2011 17:00:40                       |        |       |                   |          |                                     |     |
| ist TTA (PSI/(MMCF/D))  | 6029.99           | 05/18/2011 17:00:40                       |        |       |                   |          |                                     |     |
| (*************************************                                  | 0029.99           | 03/10/2011 17:00:40                       |        |       |                   |          |                                     |     |
|   |                   |   |        |       |                   |          |                                     |     |
|   | г                 | Nate Created: 11/26/2013 8:06:38 AM       |        |       |                   |          | Date Created: 11/26/2013 8:06:38 AM |     |
| Productivity Qgas   |                   |   | 1      | -     | -                 | TTA Qgas |                                     | -   |
| ÷-1   |                   |   |        |       | 6000              | 1        |                                     |     |
| E I   |                   |   |        | -     | 5500              |          |                                     |     |
|   |                   |   |        | 11000 | E                 |          |                                     | -11 |
|   |                   |   |        |       | 5000              |          |                                     |     |
|   |                   |   |        | -     | 4500              |          | /                                   |     |
| <b>€}</b> ;;  |                   |   |        |       | Ē                 | 1        |                                     | -91 |
|   |                   |   |        |       | 4000              | ··· †    | ·····                               |     |
|   |                   |   |        | 8000  | (Q/JJWW)/<br>3500 |          |                                     |     |
|   |                   |   |        |       |                   |          |                                     | -7  |
|   |                   |   |        | -     | 3000              |          |                                     |     |
|   |                   | × `                                       |        | 6000  | 2500              |          |                                     |     |
|   |                   | <u></u>                                   |        |       | E                 |          |                                     | -   |
|   |                   |   |        | -5000 | 2000              |          |                                     |     |
| F I I   |                   |   |        |       | F                 | 1        |                                     | = . |
|   |                   |   |        | 4000  | 1500              |          |                                     |     |
|   |                   |   |        | 4000  | E                 | 7        |                                     |     |
|   |                   |   |        | 4000  | 1500              | 1        |                                     |     |
|   |                   | Date-Time - DateTime                      | 15 Sun |       | E                 | 8        | Sun Date-Time - Date Time 15 Sun    |     |

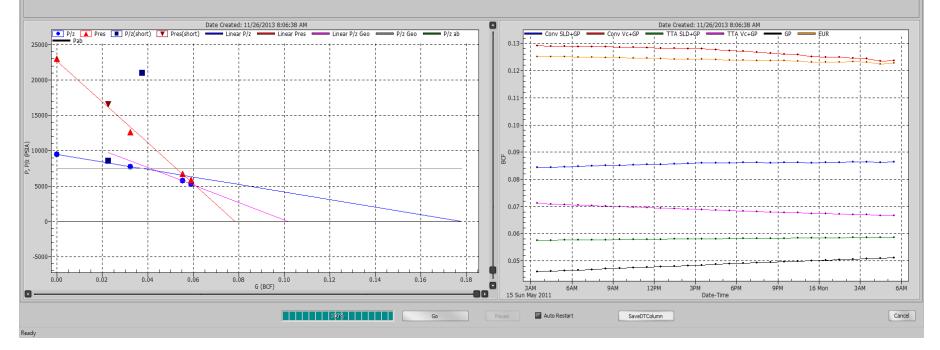
# DOT – P/z and MBAL/EBAL

### 🚾 x64 Well Analyzer - C:\WORK\RT Software Demos\DOT #1 - UHPHT GOM using outBHP.ProData - [Real Time Testing]

- File Memory Analysis Plot View Tools Help

### Inputs Summary Outputs

| Summary PBU DD P    | TA/ Productivity | HC Volumes      | P/z (  | Derivative 0 | ilWaterRates | Analysis Events |                     |              |                       |                     |                           |           |          |             |
|---------------------|------------------|-----------------|--------|--------------|--------------|-----------------|---------------------|--------------|-----------------------|---------------------|---------------------------|-----------|----------|-------------|
| Date Time           | Gas<br>Produced  | PBU<br>Duration | Pres   | z-Factor     | P/z          | GIP SLD @P=0    | GIP SLD<br>@P ab=15 | GIP P/z @P=0 | GIP P/z<br>@P/z ab=15 | GIP P/z geo<br>@P=0 | GIP P/z geo<br>@P/z ab=15 | m Pres    | m Pz     | m Pz<br>Geo |
| MM/dd/yyyy HH:mm:ss | BCF              | HOURS           | PSIA   | dimless      | PSIA         | BCF             | BCF                 | BCF          | BCF                   | BCF                 | BCF                       | PSIA/BCF  | PSIA/BCF | PSIA/BC     |
| 01/01/0001 00:00:0  | 0.00             |                 | 23000  | 2.434        | 9449.        | NaN             | NaN                 | NaN          | NaN                   | NaN                 | NaN                       | -99999.0  | -99999.0 | -99999      |
| 05/04/2011 20:23:49 | 0.02             | 1               | 16540  | 1.938        | 8532.2       | NaN             | NaN                 | NaN          | NaN                   | NaN                 | NaN                       | -99999.0  | -99999.0 | -999999.    |
| 05/12/2011 04:55:1  | 0.03             | 154             | 12629  | 1.633        | 7734.        | 0.1             | 0.1                 | 0.2          | 0.2                   | 0.1                 | 0.1                       | -320740.1 | -53036.1 | -10607      |
| 05/13/2011 16:27:40 | 0.04             | 13              | 632187 | 30.157       | 20963.       | 0.1             | 0.1                 | 0.2          | 0.2                   | 0.1                 | 0.1                       | -320740.1 | -53036.1 | - 106072    |
| 05/17/2011 13:03:4  | 0.06             | 7               | 6754   | 1.181        | 5717.        | 0.1             | 0.1                 | 0.2          | 0.2                   | 0.1                 | 0.1                       | -295835.6 | -53036.1 | -10607      |
| 05/18/2011 19:02:2  | 0.06             | 2               | 5880   | 1.119        | 5254.        | 0.1             | 0.1                 | 0.2          | 0.2                   | 0.1                 | 0.1                       | -290040.1 | -53036.1 | -12294      |



\_ 0 \_X

### **DOT - Conclusions**

### \* It's WEE!

\* Gosh, we wasted a lot of rig time...

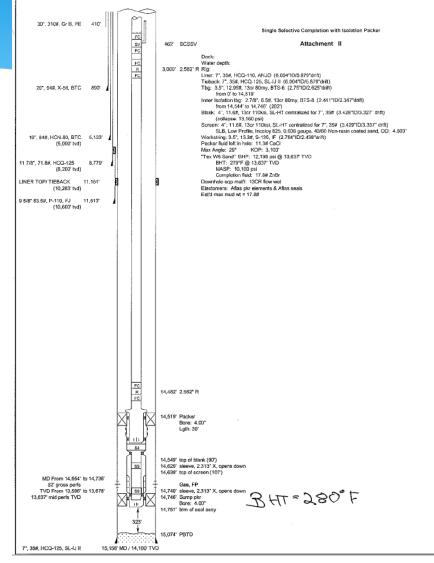
# GOM Volatile Oil Well

### \* Start-up: Objectives

- \* Figure Out kh & skin
- \* Determine Productivity
- \* Determine Oil-in-Place
- \* Estimate Recovery

Objective: Does an injection well make sense?

### Fizzy - WBD



### Fizzy-1 Logs



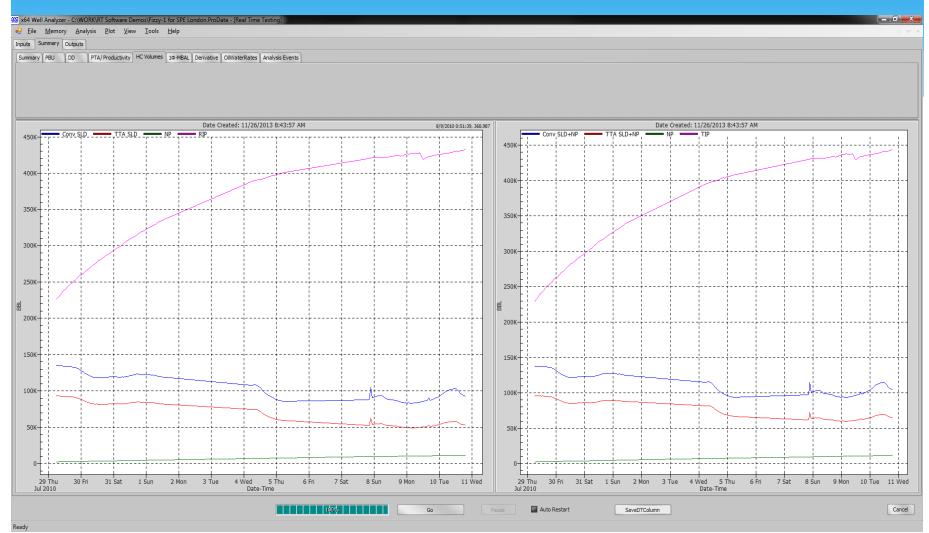
# Fizzy - Summary

| File  |                                 | Software Demos\Fizzy-1 for \$ | SPE London              | .ProData - [R | Real Time Te                          | sting]         |                 |      | _    | _    |                        |            | _  | _             |               |             |                  |                    |                       |       |   |   |
|---|---------------------------------|-------------------------------|-------------------------|---------------|---------------------------------------|----------------|-----------------|------|------|------|------------------------|------------|--|---------------|---------------|-------------|------------------|--------------------|-----------------------|-------|---|---|
|   |                                 | Plot View Tools Helj          | р                       |               |                                       |                |                 |      |      |      |                        |            |  |               |               |             |                  |                    |                       |       |   |   |
|   | Summary Outputs                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            |  |               |               |             |                  |                    |                       |       |   |   |
| Summa   | Y PBU DD PTA/P                  | roductivity HC Volumes 1Φ-    | MBAL Deriv              | ative OilWat  | terRates A                            | nalysis Events |                 |      |      |      |                        |            |  |               |               |             |                  |                    |                       |       |   |   |
|   | Start D/T<br>ddMmmyyyy hh:mm:ss | End D/T<br>ddMmmyyyy hh:mm:ss | Test<br>Length<br>Hours | Test<br>Type  | WHPi<br>psia                          |                | DHGPi (<br>psia |      |      |      | Qoil_i Qo<br>BBL/D BBI |            | Skin   | DPskin<br>psi | PStar<br>psia | PI Eff<br>% | DPs/Q<br>psi/BBL | Report Link        | Graph Link            |       |   |   |
| 1   | 25Jul2010 15:40:35              | 27Jul2010 16:51:19            | 49.18                   | DD            | 6252                                  | 5736           | -1              | -1   | 9903 | 9341 | 0                      | 725 39.7   | 3.3  | 134           | 9177          | 65          | 0.19             | RTRep 2010Jul25 15 | 403 RTRep 2010Jul25   | 15403 |   |   |
|   |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            |  |               |               |             |                  |                    |                       |       |   |   |
|   |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            |  |               |               |             |                  |                    |                       |       |   |   |
|   |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            |  |               |               |             |                  |                    |                       |       |   |   |
|   |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            |  |               |               |             |                  |                    |                       |       |   |   |
|   |                                 |                               | D                       | ate Created:  | : 11/26/20                            | 13 8:43:57 A   | AM              |      |      |      |                        |            |  |               |               |             |                  | Date Created: 1    | 11/26/2013 8:43:57 AM |       |   |   |
|   |                                 | BHP Qoil                      | 1                       |               |                                       |                |                 | 1    |      |      |                        |            |  |               | VHP -         | BHP         | Qoi              |                    |                       | 1     |   |   |
| 1000  | 0+                              |                               |                         |               |                                       |                |                 |      |      |      |                        |            |  |               |               |             |                  |                    |                       |       |   |   |
|   | 12 7                            |                               |                         |               | ]                                     |                |                 |      |      |      |                        |            | 10000  | )<br>         |               |             |                  |                    |                       |       |   |   |
|   |                                 |                               |                         |               | 1                                     |                |                 |      |      |      |                        |            |  | E             |               |             |                  |                    |                       |       |   | 1 |
| 900   |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            | 9000   | E             |               |             |                  |                    |                       |       |   |   |
|   | 0                               |                               |                         |               |                                       |                |                 |      |      |      |                        | -700       | 9000   |               |               |             |                  |                    |                       |       |   |   |
|   | 0                               |                               |                         |               |                                       |                |                 |      |      |      |                        | _          |  |               |               |             |                  |                    |                       |       |   |   |
| 800   | 0                               |                               |                         |               |                                       |                |                 |      |      |      |                        | <br>       | 9000<br>8000   |               |               |             |                  |                    |                       |       |   |   |
| 800   | 0                               |                               |                         |               |                                       |                |                 |      |      |      |                        | _          | 9000   |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700                                    |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        | 600<br>500 | 9000<br>8000<br>7000                                 |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700                                    |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        | <br>       | 9000<br>8000<br>7000                                 |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700                                    | 0                               |                               |                         |               | · · · · · · · · · · · · · · · · · · · |                |                 |      |      |      |                        | 600<br>500 | 9000<br>8000<br>7000                                 |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700<br>600                             | 0                               |                               |                         |               |                                       |                |                 |      |      |      |                        |            | 9000<br>8000<br>7000<br>7000                         |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700<br>600                             |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            | 9000<br>8000<br>7000<br>7000                         |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700<br>600<br>500<br>400               |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            | 900(<br>800(<br>700(<br>500(                         |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700<br>600<br>500<br>400               |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        | 600<br>    | 900(<br>800(<br>700(<br>500(                         |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700<br>600<br>500<br>400<br>300        |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        |            | 9000<br>8000<br>7000<br>5000<br>4000<br>3000         |               |               |             |                  |                    |                       |       |   |   |
| 900<br>800<br>700<br>600<br>500<br>400<br>300 |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        | 600<br>    | 9000<br>8000<br>7000<br>5000<br>4000                 |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700<br>600<br>500<br>400<br>300        |                                 |                               |                         |               |                                       |                |                 |      |      |      |                        | 600<br>    | 9000<br>8000<br>7000<br>5000<br>4000<br>3000         |               |               |             |                  |                    |                       |       |   |   |
| 800<br>700<br>600<br>500<br>400<br>300        |                                 |                               | 1 5                     | in Dati       | e-Time - Dia                          | iteTime        |                 | 8 Su |      |      |                        | 600<br>    | 9000<br>8000<br>7000<br>5000<br>4000<br>3000<br>2000 |               |               |             |                  | 1 Sun              | Time - DateTime       | 8 Su  | n |   |
| 800<br>700<br>600<br>500<br>400<br>300<br>200 |                                 |                               | 1 50                    | in Dati       | e-Time - De                           | teTime         |                 | 8 Su | un   |      |                        | 600<br>    | 9000<br>8000<br>7000<br>5000<br>4000<br>3000<br>2000 |               |               |             |                  | 1 Sun Date-        | Time - Date Time      | 8 Su  |   |   |

# Fizzy - Productivity

| al Pres (PSIA)<br>: PBU DPskin/Q (PSI/(BBL/D))<br>: DD DPskin/Q (PSI/(BBL/D))   |               | vative OlWaterRates Analysis Events 01/01/0001 00:00:00 07/27/2010 16:51:19 | x     |     |          |              |              |                                       |         |          |
|---|---------------|---|-------|-----|----------|--------------|--------------|---------------------------------------|---------|----------|
| nry PBU DD [PTA/Productivity] HC Volumes<br>al Pres (PSIA)<br>: PBU DPskin/Q (PSI/(BBL/D))<br>: DD DPskin/Q (PSI/(BBL/D)) | 0<br>0<br>.19 | 01/01/0001 00:00:00   | •     |     |          |              |              |                                       |         |          |
| al Pres (PSIA)<br>: PBU DPskin/Q (PSI/(BBL/D))<br>: DD DPskin/Q (PSI/(BBL/D))   | 0<br>0<br>.19 | 01/01/0001 00:00:00   |       |     |          |              |              |                                       |         |          |
| : PBU DPskin/Q (PSI/(BBL/D))<br>: DD DPskin/Q (PSI/(BBL/D))   | 0<br>.19      |   | ·     |     |          |              |              |                                       |         |          |
| :DD DPskin/Q (PSI/(BBL/D))  | .19           |   |       |     |          |              |              |                                       |         |          |
|   |               |   | •     |     |          |              |              |                                       |         |          |
| ((517)  |               | 01/01/0001 00:00:00   |       |     |          |              |              |                                       |         |          |
| Productivity Q/DP (BBL/D/PSI)   | 0.421         | 08/12/2010 16:30:25   |       |     |          |              |              |                                       |         |          |
|   | 2372.92       | 08/12/2010 16:30:25   | •     |     |          |              |              |                                       |         |          |
|   |               |   |       |     |          |              |              |                                       |         |          |
|   |               |   |       |     |          |              |              |                                       |         |          |
|   |               |   |       |     |          |              |              |                                       |         |          |
|   |               |   |       |     |          |              |              |                                       |         |          |
|   |               |   |       |     |          |              |              |                                       |         |          |
|   | C             | ate Created: 11/26/2013 8:43:57 AM  |       |     |          |              | Date Creater | d: 11/26/2013 8:43:57 AM              |         |          |
| Productivity QOil   |               |   |       |     | 2400     | TTA QOI      |              |                                       |         |          |
| [ <b>\</b>  |               |   | ·     |     |          | _            |              |                                       |         | 7        |
| <u> </u>  |               |   |       |     | 2200     |              |              |                                       | <u></u> |          |
| E   |               |   |       |     | 2000     |              |              |                                       | ·       |          |
| Į   |               |   |       |     | -        |              |              |                                       |         |          |
| ļ   |               |   |       |     | 1800     |              |              | /                                     | 1       | -5       |
| E I 🔪   |               |   |       |     |          |              |              |                                       |         |          |
|   |               |   |       |     |          |              |              |                                       |         | -4       |
| E   |               |   |       | -3  | <u>a</u> |              |              |                                       |         | -3       |
|   |               |   |       |     | 1200     |              |              |                                       |         |          |
| E   |               |   |       |     | 0        |              |              |                                       |         | -2       |
|   |               |   |       |     | 1000     | ~            |              |                                       |         |          |
| E   |               |   |       |     | 800      |              |              |                                       |         |          |
|   |               |   |       |     |          | -m-          |              |                                       |         |          |
| E   |               | •   |       | t   | 600      | ·····        | <b>bb</b>    | · · · · · · · · · · · · · · · · · · · |         | <b>_</b> |
| ug 2010   | 1 Sun         | Date-Time - DateTime  | 8 Sun |     | Aug 2010 |              | 1 Sun<br>Dat | te-Time - DateTime                    | B Sun   |          |
|   |               |   |       |     |          |              |              |                                       |         |          |
|   |               |   | 100%  | 134 | Pause 4  | Auto Restart | SaveDTColumn |                                       |         | Cano     |

# Fizzy – Flowing MBAL/EBAL



135

# Fizzy - Conclusions

- \* Only about 450,000 STB in place
- \* Around 100,000 recoverable by natural drive
- \* Maybe 200,000 more recoverable with water injection
- \* Don't drill \$30 MM injector

## Nordzee #1

- \* Gas Well with Subsea Tree
- \* "Single Zone"? reservoir, but with possible baffles
  - MDTs match gas gradient
- \* Not fully cleaned-up during initial completion test

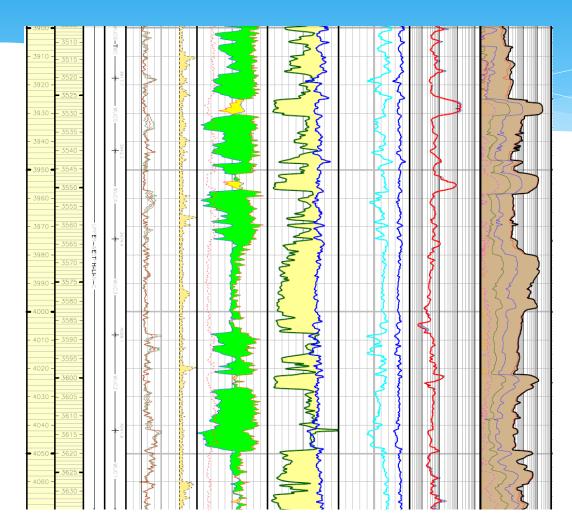
\* Objectives:

- \* Determine skin/perm
- \* Determine in-place HCs
- \* Estimate Recovery

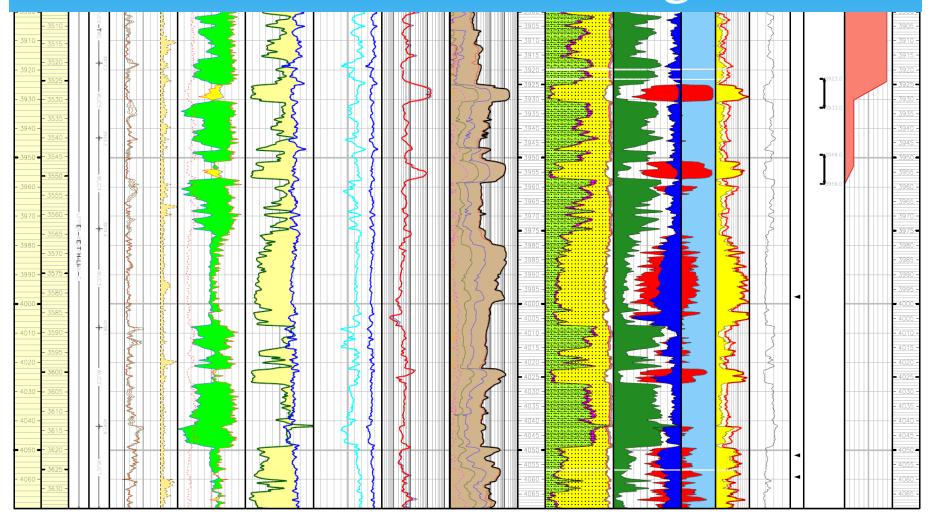
### Nordzee #1 WBD

| RT/TH HOP. : 73.675 r                  | Neble Al White //                        | OP-Rettage des TU                                | ANNULUS         | 1105.        |             |                             |                    |        |                  |         |
|--|--|--|-----------------|--------------|-------------|-----------------------------|--------------------|--------|------------------|---------|
| RI/TH HOP /3.6/31                      | I. NODIE AI WHITE (H                     | OF-Bolloming (H)                                 |                 | CIBRINE S    | G 1.03      |                             |                    |        |                  |         |
| COMPLETION DATE :                      |  |  |                 |              |             |                             |                    |        |                  |         |
|  | OLUMES                                   |  | DRILLING D      | EPTHS/RT     |             |                             |                    |        |                  |         |
| 7"Vam Top riser to RT<br>TUBING VOLUME | volume                                   | 1.35 M3<br>15.67 M3                              | 700 70 100      | R HANGER :   | 0704.54     | 07                          |                    |        |                  |         |
| 4.5"LINER VOLUME                       |  | 4.99 M3  |                 | 1/2" LINER H |             |                             |                    |        |                  |         |
| 3.5"x 7"ANNULUS VOI                    | UME till PKR                             | 0.33 M3  | TRSCSSV         | olume 9000   | >0 psi = ~2 | 50 ml (2 ree                | s 200m)            |        |                  |         |
|  |  | API / 10000 psi rated working pre                |                 |              |             |                             | · · · ·            |        |                  | 15      |
|  |  |  |                 |              |             |                             |                    |        |                  |         |
| TUBING HANGER<br>X-MASTREE             |  | FMC 13 5/8"x 4.5" w/ 3.925" S<br>FMC JXT-3       | RP PROFILE      |              |             |                             |                    |        |                  |         |
| N-MASTREE<br>PMV production maste      | - unius                                  | FMC JXT-3<br>5°1/8 10K                           |                 |              |             |                             |                    |        |                  |         |
| PSV production swab v                  | alve                                     | 5"1/8 10K  |                 |              |             |                             |                    |        |                  |         |
| PMV production wing v                  |  | 5"1/8 10K  |                 |              | length      | To bottom o                 | ofitem             |        |                  |         |
| Annullus valves                        |  | 2"1/16 10K                                       |                 |              | ofitem      |                             |                    |        | Original         |         |
|  |  | STRING   |                 |              | Length      | Depth                       | Depth              | ID.    | Drift            |         |
| ITEM QTY (                             | ESIGNATION                               |  | all length to b | bottom       | m.          | mRT                         | mŤH                | inches | inches           | 11      |
| 1 1 TBG                                | HANGER 13"5/8 X                          | S" VAN TOP HC                                    |                 | HOP -        | NAW         | 73.765                      | 0.00               | HOP    | 3,875"           | /  ⊢    |
| 2 1 PUP.                               | IOINT 5" VAM TOP                         | HC 12.6# C-95 13%Cr PIN X PIN                    | N               | HUF =        | 1.84        | 75.61                       | 1.84               | 3,958" | drift            | 4 11    |
| 3 1 XO 4                               | 5" VTOP box 12 6# 3                      | (3.5" VTOP 9.2# pin13% CR 1-8                    | 0               |              | 0.95        | 76.56                       | 2.79               | 3,958" | 3,875"           |         |
| 4 2 PUP.                               | IOINT 4"1/2 VAM TO                       | OP 12.6# C-95 13%Cr                              |                 |              | 6.40        | 82.96                       | 9.19               | 3,958" | 3,875"           |         |
|  |  |  |                 |              |             |                             |                    |        |                  |         |
| 5 7 TUBI                               | ICC 4"1/2 VAM TOD                        | 12.6# C-95 13%CR                                 |                 |              | 90.31       | 173.27                      | 99.50              | 3.958" | 3,875"           |         |
|  | 100 H 1/2 VAINI TUP                      | 12.0# 0-80 13 /sUR                               |                 |              | 30.31       | 113.21                      | 88.00              | 3,808  | 3,615            |         |
| 6 1 PUP.                               | IOINT 4"1/2 VAM TO                       | OP 12.6# C-95 13%Cr                              |                 |              | 1.96        | 175.23                      | 101.46             | 3,958" | 3,875"           |         |
| 7 1 BAKE                               | R TME 6.5 TRSCS                          | V W/ NIPPLE ADAPTER 3.812                        | " BA PROFILE    |              | 2.03        | 177.26                      | 103.49             | 3,812" | n/a              |         |
| 8 1 PUP.                               | IOINT 4"1/2 VAM TO                       | OP 12.6# C-95 13%Cr                              |                 | _            | 1.43        | 178.69                      | 104.92             | 3,958" | 2.867"           |         |
|  | 0.414.00.1/10.00                         | 0.011.0.05.4001.55                               |                 |              |             |                             |                    |        | Drift            |         |
| 9 1 TUBI                               | IG 4"1/2 VAM TOP 1                       | 2.0# C-95 13%CR                                  |                 |              | 13.28       | 191.97                      | 118.20             | 3,958" | Nylon            |         |
| 10 1 PUP.                              | OINT 4"1/2 VAM TO                        | OP 12.6# C-95 13%Cr                              |                 |              | 1,96        | 193.93                      | 120.16             | 3.958" |                  |         |
| 11 1 XO 4.                             | 5" VTOP box 12.6# >                      | 3.5" VTOP 9.2# pin13% CR L-8                     | 10              |              | 0.54        | 194.47                      | 120.70             | 2.992" |                  |         |
| 12 1 PUP.                              | OINT 3.5" VAMTOR                         | 9.2# 13% CR L-80                                 |                 |              | 1.48        | 195.95                      | 122.18             | 2.992" | ↓ I              |         |
|  |  |  |                 |              |             |                             |                    |        | 2 867"           |         |
| 13 255 TUBI                            | USS 3.5" VAMIOP 9                        | .2# 13% CR L-80 R-3                              |                 |              | 3171.67     | 3367.62                     | 3293.85            | 2.992" | 2.867"           |         |
| 14 1 PUP.                              | OINT 3.5" VANTOR                         | 9.2# 13% CR L-80                                 |                 |              | 1.96        | 3369.58                     | 3295.81            | 2.992" | 2 867"           |         |
|  |  | (3.5" VTOP 9.2# pin13% CR L-8                    | 0               |              | 0.53        | 3370.11                     | 3296.34            | 2.992" | 2.867"           |         |
| 16 1 PUP.                              | OINT 4"1/2 VAM TO                        | DP 12.6# C-95 13%Cr                              |                 |              | 2.96        | 3373.07                     | 3299.30            | 2.992" | 2.867"           | 1 11    |
|  | R SS-175GAUGE C                          |  |                 |              | 1.67        | 3374.74                     | 3300.97            | 2.992" | 2.867"           |         |
|  |  | OP 12.6# C-95 13%Cr                              |                 |              | 1.92        | 3376.66<br>3377.19          | 3302.89<br>3303.42 | 2.992" | 2.867"           | 4 11    |
|  |  | 3.5" VTOP 9.2# pin13% CR L-8<br>9.2# 13% CR L-80 | su              |              | 1.48        | 3377.19                     | 3303.42            | 2.992  | 2.867            |         |
| 21 1 TUBI                              | G 3.5" VAMTOP 9.2                        | # 13% CR L-80 R-3                                |                 |              | 12.50       | 3391.17                     | 3317.40            | 2.992" | 2.867"           |         |
|  | OINT 3.5" VAMTOR                         |  |                 |              | 1.97        | 3393.14                     | 3319.37            | 2.992" | 2.867"           |         |
| 23 1 BAKE                              | R 2.812" AOF NIPP                        | LE 9.2# VAMTOP 13%Cr L-80                        |                 |              | 0.69        | 3393.83                     | 3320.06            | 2.81"  | n/a              |         |
| 24 1 PUP.                              | ioint 3.5" vamtor                        | 9.2# 13% CR L-80                                 |                 |              | 1.46        | 3395.29                     | 3321.52            | 2.992" | 2.867"           |         |
|  |  | # 13% CR L-80 R-3                                |                 |              | 12.47       | 3407.76                     | 3333.99            | 2.992" | 2.867"           |         |
|  | OINT 3.5" VAMTOR                         | 3.5" VTOP 9.2# pin13% CR L-80                    | 0               |              | 0.53        | 3409.73<br>3410.26          | 3335.96<br>3336.49 | 2.992" | 2.867"<br>2.867" | /  ⊢    |
|  | R SB-3 PACKER                            | (3.5 VIOI 8.2# pilli3/8 OK E-6                   |                 |              | 1.21        | 3411.47                     | 3337.70            | 2.992" | 2.867"           |         |
|  |  | OP 12.6# C-95 13%Cr                              |                 |              | 1.78        | 3413.25                     |                    | 2.992" | 2.867"           |         |
| 30 1 XO 4.                             | 5" VTOP box 12.6# >                      | 3.5" VTOP 9.2# pin13% CR L-8                     | 0               |              | 0.53        | 3413.78                     | 3340.01            | 2.992" | 2.867"           |         |
| 31 1 PUP.                              | IOINT 3.5" VAMTOR                        | 9.2# 13% CR L-80                                 |                 |              | 1.48        | 3415.26                     | 3341.49            | 2.992" | 2.867"           |         |
| 32 1 TUBI<br>33 1 PUP                  | IG 3.5" VAMTOP 9.2<br>IOINT 3.5" VAMTOP  | # 13% CR L-80 R-3                                |                 |              | 12.50       | 3427.76<br>3429.73          | 3353.99<br>3355.96 | 2.992" | 2.867"<br>2.867" |         |
|  |  | LE 9.2# VAMTOP 13%Cr L-80                        |                 |              | 0.98        | 3429.73                     | 3355.90            | 2.992  | 2.807<br>n/a     | ⊢       |
| 35 1 PUP                               | IOINT 3.5" VAMTOR                        | 9.2# 13% CR L-80                                 |                 |              | 1.47        | 3432.18                     | 3358.41            |        | 2.867"           | /  ⊩    |
| 36 1 PUP.                              | IOINT 3.5" VAMTOR                        | 9.2#13% CR L-80                                  |                 |              | 1.92        | 3434.10                     | 3360.33            | 2.992" | 2.867"           |         |
| 37 1 XO 3.                             | 5" VTOP BOX 9.2# 1                       | 3% CR L-80 x 4.5" VTOP pin 12                    |                 |              | 0.53        | 3434.63                     | 3360.86            |        | 2.867"           |         |
| 38 1 SELF                              | ALIGNING MULE S                          | HOE 4"1/2 VAM TOP 12,6# L-8                      | 0 13%CR 20FT    |              | 4.56        | 3439.19                     | 3365.42            | 2.992" | 2.867"           |         |
|  |  |  |                 | IN PBR       | 2.03        | <ul> <li>3441.22</li> </ul> | 3367.45            | 2.992" | 2.867"           |         |
|  |  |  |                 |              |             |                             |                    |        |                  | 1 F     |
|  |  |  |                 |              | 1           |                             |                    |        |                  |         |
|  |  |  |                 |              |             |                             |                    |        |                  |         |
|  |  |  |                 |              |             |                             |                    |        |                  |         |
|  | LINED 12.84 1 00                         |  |                 |              |             | 2420.40                     |                    | 2.050  |                  |         |
|  | LINER, 12.6#, L-80,<br>PUR joint 2952 42 | m RT - 3854.38 m RT for correl                   | lation          |              |             | 3439.10                     |                    | 3,958" |                  |         |
| 4-1/2                                  | 1 of joint 3632.43                       | in ter - 3034.30 in ter tof correl               | auvil           |              | <u> </u>    |                             |                    |        |                  |         |
| 4 1/2                                  | LANDING COLLAR                           |  |                 |              |             | ŧ                           | 4067.14            | mRT    |                  |         |
|  |  |  |                 |              |             |                             |                    |        |                  |         |
| Perforations                           |  |  |                 | Net Interval |             |                             |                    |        |                  |         |
|  | orforated from '                         | 08 till Jan 10 2013                              |                 |              |             | NOT NORM                    | CLASSIFI           | ED     |                  |         |
|  | erforated from Jan<br>879 - 3885 mRT     | 08 till Jan 10 2013<br>3805.25 - 3811.13         | mTH             | 6m           | 6 spf       | Deviation @                 | h nacker de        | oth    | 34               | degrees |
|  | 923 - 3933 mRT                           | 3849.13 - 3859.13                                |                 | 10m          | 6 spf       | Deviation @                 | D reservoir        |        |                  | degrees |
|  | 949 - 3959 mRT                           | 3875.13 - 3885.13                                |                 | 10m          | 12 spf      |                             |                    |        |                  | -0      |
|  |  |  |                 |              |             |                             |                    |        |                  |         |
| -                                      |  |  | -               |              |             | I                           |                    |        |                  |         |
|  |  |  |                 |              |             |                             |                    |        |                  |         |

## Nordzee #1 - Logs



# Nordzee #1 Full Logs



# Nordzee Summary

|   | Y PBU DD PTA/P                        | roductivity HC Volumes P/z               | Derivat                 | ive OilWate  | erRates An   | alysis Event | s             |               |              |              |                |               |                     |           |               |               |               |                   |                                     |                                   |              |       |
|---|---------------------------------------|--|-------------------------|--------------|--------------|--------------|---------------|---------------|--------------|--------------|----------------|---------------|---------------------|-----------|---------------|---------------|---------------|-------------------|-------------------------------------|-----------------------------------|--------------|-------|
|   | Start D/T<br>ddMmmyyyy hh:mm:ss       | End D/T<br>ddMmmyyyy hh:mm:ss            | Test<br>Length<br>Hours | Test<br>Type | WHPi<br>psia | WHPf<br>psia | DHGPi<br>psia | DHGPf<br>psia | BHPi<br>psia | BHPf<br>psia | QGasi<br>Mcf/D | QGas<br>Mcf/D | Perm<br>md          | Skin      | DPskin<br>psi | PStar<br>psia | PI Eff<br>%   | DPs/Q<br>psi/MMcf | Report Link                         | Graph Link                        |              |       |
|   | 17Aug2013 22:29:53                    | 18Aug2013 00:17:53                       | 1.8                     | PBU          | 4371         | 4587         | 5498          | 5598          | 5650         | 5745         | 13299          | 13299         | 119                 | 20.3      | 80            | 5769          | 26            | 6.04              | INTRop 2012Aug17 2220               | Nordzee-                          |              |       |
|   |                                       | 18Aug2013 04:35:53                       | 1.3                     | PBU          | 3991         | 4533         | 5354          | 5558          | 5519         | 5704         | 24765          | 24765         | 123.8               | 26.1      | 185           | 5770          | 22            | 7.46              |                                     | 107000 201200019 0217             |              |       |
|   |                                       | 18Aug2013 08:47:53                       | 4.2                     | DD           | 1699         | 4077         | 5604          | 5378          | 5751         | 5540         |                | 20196         | 2.2                 |           |               |               |               | -73.81            | Nordzee-<br>10.000 2012Aug19 0425   | Nordzee-<br>IBTRos 2012Aug19 0425 |              |       |
|   | ······                                | 09Sep2013 15:18:53                       | 45.4                    | PBU          | 3624         | 4214         | 4953          |               | 5113         |              | 25141          |               | 86                  | 12.1      | 125           |               | 37            | 4.99              | INTRop 201250007 1754               | Nordzee-<br>10TDop 201250007 1754 |              |       |
|   |                                       | 19Sep2013 13:28:53                       | 3.8                     | PBU          | 3591         | 4136         | 4845          |               | 5000         |              |                | 23108         | 82.7                | 10.5      |               | 5200          |               | 4.54              | 10 Then 20125ep10, 0040<br>Nordzee- | IDTDop 20125op10_0040<br>Nordzee- |              |       |
|   | · · · · · · · · · · · · · · · · · · · | 22Sep2013 11:35:53                       | 8.02                    | PBU<br>PBU   | 3514         | 3874         | 4795          |               | 4951<br>4589 |              |                | 24013         | NaN<br>96.9         | NaN<br>14 | NaN<br>176    |               |               | NaN               | 10TDop 201250p22 0224               | 10TBon 2012Eon22 0224<br>Nordzee- |              |       |
|   |                                       | 09Oct2013 06:29:53<br>09Oct2013 17:44:53 | 1.45<br>7.95            | PBU          | 2870<br>3735 | 3709<br>3776 | 4425<br>4729  | 4723<br>4697  | 4589         | 4855         |                | 30333<br>3718 | 86.8<br>NaN         | 14<br>NaN | NaN           |               | 33<br>NaN     | 8,6<br>NaN        | 10 Thop 20120ct00 0502<br>Nordzee-  | 10TDop 20120ct00_0502<br>Nordzee- |              |       |
|   | 090002013 09.47:53                    | 090012013 17.44:53                       | 7.90                    | PDU          | 3733         | 3770         | 4729          | 4097          | 4003         | 4029         | 3718           | 3718          | INdiN               | INdiN     | INdiN         | 4032          | INdIN         | NaN               | 1010200 0047                        | 10T0cs 20120ck00 0047             |              |       |
|   |                                       |  |                         | ate Created  | 1: 11/26/20  | 13 8:55:4    | 5 AM          |               |              |              |                |               | 7                   |           | r             |               |               |                   | Date Created: 11/2                  | 6/2013 8:55:45 AM                 |              | 200   |
| 0 | WHP D                                 | HGP BHP                                  | Qgas                    |              |              |              |               |               |              |              |                |               | -                   | 6000-     | W             | HP            | DHGP          | BHF               | Qgas                                |                                   |              |       |
|   | E.                                    |  |                         |              |              | 1            |               |               |              |              | 1              |               |                     |           |               | 94            |               |                   | 1                                   |                                   |              |       |
|   |                                       |  |                         |              |              |              |               |               |              |              | j              |               | -30000              | 5500-     | E             |               |               |                   |                                     | . hl                              |              | •     |
|   | £                                     | <br>                                     |                         | <u> </u>     |              | L.           |               |               |              |              | j              |               |                     | 5000-     | E             | 15            |               | -11               | h l                                 | ~~1 la ~~                         | m la company |       |
| , | F 🔁                                   |  |                         |              |              |              |               |               |              |              | <u> </u>       |               | -                   | 5000      | =             |               | $\mathcal{L}$ |                   |                                     | _                                 |              | ~     |
| ) |                                       |  |                         |              |              |              |               |               |              |              |                |               | -25000              | 4500-     | E             | 4             |               | <u> </u>          | ·····                               |                                   |              |       |
|   | E                                     |  |                         |              |              | ÷            |               |               |              |              |                |               |                     |           | E             |               | 1             |                   |                                     |                                   |              |       |
| ) |                                       |  |                         |              |              |              |               |               |              |              |                |               | -                   | 4000-     | E             |               |               |                   |                                     |                                   |              | Ξ     |
|   | EP                                    |  |                         |              |              |              |               |               |              |              | 1              |               | -20000              |           | E             | 1 m           |               |                   |                                     |                                   |              |       |
| ) |                                       | !  |                         |              |              |              |               |               |              |              |                |               |                     | 3500-     | E             |               |               |                   |                                     |                                   |              |       |
| ) | E.                                    |  |                         |              |              |              |               |               |              |              | į              |               | 3                   | < 3000-   | E             |               | į.            |                   | ····· /                             |                                   |              |       |
|   | ╘┤┝╼╲╌╌╴┤                             |  |                         |              |              | -            |               |               |              |              | 1              |               | -15000 <sup>2</sup> | ¥ 3000-   | E             |               |               |                   |                                     | y man                             |              |       |
| ) |                                       |  |                         |              |              |              |               |               |              |              | +              |               | -                   | 2500-     | E             |               |               |                   |                                     |                                   |              |       |
|   | E                                     |  |                         |              |              |              |               |               |              |              | 1              |               | 1                   |           | F             |               | 1             | - 11              |                                     |                                   |              |       |
| D |                                       |  |                         |              |              |              |               |               |              |              |                |               | 10000               | 2000-     |               | • • • • • • • |               |                   |                                     |                                   |              | • - • |
|   | E                                     |  |                         |              |              |              |               |               |              |              |                |               | -10000              | 1500      | E III         |               |               |                   |                                     |                                   |              |       |
| ) | E                                     |  |                         |              |              |              |               |               |              |              | ]              |               |                     | 1500-     | E             |               |               |                   |                                     |                                   |              |       |
| D | F                                     | į.                                       |                         |              |              |              |               |               |              |              |                |               |                     | 1000-     | E             |               |               |                   |                                     |                                   |              |       |
|   | E                                     | i i                                      |                         |              |              |              |               |               |              |              | 1              | -             | -5000               |           | Ē             |               |               |                   |                                     |                                   |              |       |
| 0 | ╶╪╶╟┾╴╴╴╴╴╴╴╴                         |  |                         |              |              |              |               |               |              |              |                |               |                     | 500-      | <u></u>       |               |               |                   |                                     |                                   |              |       |
|   | E                                     |  |                         |              |              | 1            |               |               |              |              | 1              |               |                     |           | E             |               | 1             |                   |                                     |                                   |              |       |
| ľ | +                                     |  |                         |              |              | ·            |               |               |              |              | <br>           |               | -0                  | 0-        | ╞╴╴╝╾╾║       | WU            |               | k                 |                                     |                                   |              | •     |
|   | 15 T<br>Oct 2013                      | ue 22 Tu                                 | e                       |              | -Time - Dat  | 1 Fri        |               | 8 Fri         |              | 1            | 5 Fri          |               |                     |           | )13           |               | Sep           |                   | Oc<br>Date-Time -                   |                                   | Nov          |       |

# Nordzee Productivity

| x64 Well Analyzer - C:\WORK\RT Software Demos\  | NordZee #1 Ex.ProD | ata - [Real Time Testing]              |              |              |              |                |                           |          | - 0 - X |
|---|--------------------|--|--------------|--------------|--------------|----------------|---------------------------|----------|---------|
| <u>File Memory Analysis Plot View Transport</u> |                    |  |              |              |              |                |                           |          | - 9     |
| nputs Summary Outputs                           |                    |  |              |              |              |                |                           |          |         |
| Summary PBU DD PTA/Productivity HC Vo           | olumes P/z Deri    | ivative OilWaterRates Analysis Events  |              |              |              |                |                           |          |         |
| Initial Pres (PSIA)                             | 0                  |  |              |              |              |                |                           |          |         |
| Last PBU DPskin/Q (PSI/(MMCF/D))                | NaN                | 10/09/2013 17:44:53                    | •            |              |              |                |                           |          |         |
| Last DD DPskin/Q (PSI/(MMCF/D))                 | -73.81             | 08/18/2013 08:47:53                    | •            |              |              |                |                           |          |         |
| Last P* (PSIA)                                  | 4852               | 10/09/2013 17:44:53                    | •            |              |              |                |                           |          |         |
| Last Productivity Q/DP (MCF/D/PSI)              | 14.9               | 11/19/2013 09:09:53                    | •            |              |              |                |                           |          |         |
| Last TTA (PSI/(MMCF/D))                         | 67.29              | 11/19/2013 09:09:53                    | •            |              |              |                |                           |          |         |
|   |                    |  |              |              |              |                |                           |          |         |
|   |                    |  |              |              |              |                |                           |          |         |
|   |                    | Date Created: 11/26/2013 8:55:45 AM    |              |              |              | Date Creat     | ed: 11/26/2013 8:55:45 AM |          |         |
| Productivity Qgas                               |                    |  | 1            | -            | CTA Qgas     |                | 1                         | 1        | -       |
|   |                    |  |              | -32000 65-   | - <b> </b>   |                |                           |          | 32000   |
| 80  |                    |  |              |              |              |                |                           |          |         |
|   |                    | Δ.                                     | 1            |              |              |                | ۸.                        |          |         |
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|   |                    |  | w            | 45           | [ <b> </b>   |                | ,, <u>/</u>               | <u>W</u> |         |
|   |                    |  | New Street   | 28000 MGF/W/ |              |                |                           |          | -28000  |
| 50  |                    | ····· <b>N</b>                         | ~~~~         | MCF/D        |              | ~              | //                        |          |         |
|   |                    |  | Nr.          | 27000 2 35   | [ <b>\</b>   |                |                           |          | = 27000 |
| 40  |                    |  |              |              |              |                |                           | l h      |         |
| ·   |                    |  | 1            | -26000 30    |              | /              |                           |          |         |
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|   | M.                 | $\sim$                                 |              | -23000       |              | ~ ~            |                           |          | -23000  |
| Sep   |                    | Oct<br>Date-Time - DateTime            | Nov          | 10-          | Sep          |                | Oct<br>-Time - DateTime   | Nov      |         |
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|   |                    | 14                                     | Go Go        | Pause        | Auto Restart | SaveDTColumn   |                           |          | Cancel  |
| dy  |                    |  |              | 142          |              |                |                           |          |         |

# Nordzee – Running MBAL/EBAL

x64ODSI-Well Analyzer - C:\WOR

Ready

- 0 X

| mary PBU DD PT                                   | A/ Productivity | HC Volumes          | P/z        | Derivative Oi | WaterRates  | Analysis Events |                     |              |                       |                      |                           |            |              |                 |          |
|--|-----------------|---------------------|------------|---------------|-------------|-----------------|---------------------|--------------|-----------------------|----------------------|---------------------------|------------|--------------|-----------------|----------|
| te Time  | Gas<br>Produced | PBU<br>Duration     | Pres       | z-Factor      | P/z         | GIP SLD @P=0    | GIP SLD<br>@P ab=15 | GIP P/z @P=0 | GIP P/z<br>@P/z ab=15 | GIP P/z geo<br>@P=0  | GIP P/z geo<br>@P/z ab=15 | m Pres     | m Pz         | m Pz<br>Geo     |          |
| 1/dd/yyyy HH:mm:ss                               | BCF             | HOURS               | PSIA       | dimless       | PSIA        | BCF             | BCF                 | BCF          | BCF                   | BCF                  | BCF                       | PSIA/BCF   | PSIA/BCF     | PSIA/BC         |          |
| /01/0001 00:00:0                                 | 0.000           |                     | 5775       | 1.093         | 5283.2      |                 |                     |              |                       |                      |                           |            |              |                 |          |
| /18/2013 00:05:53                                | 0.008           | 2                   | 5770       | 1.093         | 5280.21     |                 |                     |              |                       |                      |                           |            |              |                 |          |
| /18/2013 04:29:53                                | 0.011           | 1                   | 5770       | 1.093         | 5280.63     |                 |                     |              |                       |                      |                           |            |              |                 |          |
| /09/2013 15:18:53                                | 0.560           | 45                  | 5361       | 1.063         | 5041.18     |                 |                     |              |                       | ·····                |                           |            |              |                 |          |
| /19/2013 13:28:53                                | 0.786           | 4                   | 5200       | 1.052         | 4941.92     |                 |                     |              |                       |                      |                           |            |              |                 |          |
| 22/2013 11:35:53                                 | 0.848           | 8                   | 5166       | 1.050         | 4920.79     |                 |                     |              |                       |                      |                           |            |              |                 |          |
| 09/2013 06:29:53                                 | 1.304           | 1                   | 4892       | 1.031         | 4743.08     |                 |                     |              |                       |                      |                           |            |              |                 |          |
| D/z Droc   |                 |                     |            |               |             | linear Dres     | Linear D/z Goo      | P/z Geo      | D/z ph                |                      | Conv SI D+GP              | Conv Vc+GP |              | 2014 4:53:01 PM |          |
| 💌 P/z 🔺 Pres                                     | P/z(sn          | oru) 💌 P            | res(short) | Line          | ar P/z      | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                |                      | Conv SLD+GP               | Conv Vc+GP | TTA SLD+GP   | TTA Vc+GP       | GP EUR   |
|  | P/Z(sn          | ort) [ <b>•</b> ] P |            | Line          | ar P/z      | Linear Pres     | — Linear P/z Geo    | P/z Geo      | P/z ab                | 18                   | onv SLD+GP                | Conv Vc+GP | TTA SLD+GP   | TTA Vc+GP       | GP EUR   |
|  | P/z(sn          | orc) (• P           |            | Une           |             | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                |                      | onv SLD+GP                | Conv Vc+GP | TTA SLD+GP = | TTA Vc+GP       | GP — EUR |
| 00 Pab<br>00 00 00 00 00 00 00 00 00 00 00 00 00 | P/z(sn          |                     |            | Line          | ear P/z     | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18                   |                           | Conv Vc+GP |              | TTA VC+GP       | GP EUR   |
| 00 Pab   | P/z(sn          |                     |            |               | ar P/z      | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18                   | onv SLD+GP                | Conv Vc+GP | TTA SLD+GP   |                 | GP EUR   |
| 00 Pab.<br>00                                    | P/2(sn          |                     |            |               | ar P/z<br>■ | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18<br>16<br>14<br>12 |                           | Conv Vc+GP |              |                 |          |
| 00 - Pab.  | P/2(sn          |                     |            |               | ar P/z      | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18<br>16<br>14<br>12 |                           | Conv Vc+GP |              |                 |          |
| 000 Pab.<br>000                                  | P/2(sn          |                     |            | Line          | ar P/z      | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18<br>16<br>14<br>12 |                           | Conv Vc+GP |              |                 | GP - EUR |
| 900 Pab.<br>500<br>500<br>500<br>500             | P/Z(sn          |                     |            |               | ▼           | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18<br>16<br>14<br>12 |                           | Conv Vc+GP |              |                 | GP EUR   |
| 900 - Pab.<br>900 - Pab.<br>900                  | • • • / 2(sn    |                     |            |               | ar P/z      | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18<br>16<br>14<br>12 |                           | Conv Vc+GP |              |                 |          |
| 900 Pab.<br>500<br>500<br>500<br>500<br>500      |                 |                     |            |               | ar P/z      | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18<br>16<br>14<br>12 | prv SLD+GP                | Conv Vc+GP |              |                 | GP EUR   |
|  |                 |                     |            |               | ■           | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18<br>16<br>14<br>12 | priv SLD+GP               | Conv Vc+GP |              |                 | GP EUR   |
|  |                 |                     |            |               | ■           | Linear Pres     | Linear P/z Geo      | P/z Geo      | • P/z ab              | 18<br>16<br>14<br>12 |                           | Conv Vc+GP |              |                 | GP - EUR |
|  |                 |                     |            |               | ¥           | Linear Pres     | Linear P/z Geo      | P/z Geo      | P/z ab                | 18<br>16<br>14<br>12 |                           | Conv Vc+GP |              |                 | GP - EUR |
| 000 Pab.<br>000                                  |                 |                     |            |               | ar P/2      | Linear Pres     | Linear P/z Geo      | P/z Geo      |                       | 18<br>16<br>14<br>12 | I Sun 85                  |            |              | ТТА VC+GP       | CP EUR   |

## Nordzee - Conclusion

- Early PBUs occurred when well was still cleaning up accurate for what was flowing at the time, but not whole zone
- \* No good drawdowns
- \* PBU perms around 85 md, with a skin around 13
- \* Apparently 15 BCF hydraulically connected
- \* At least 8 BCF recoverable

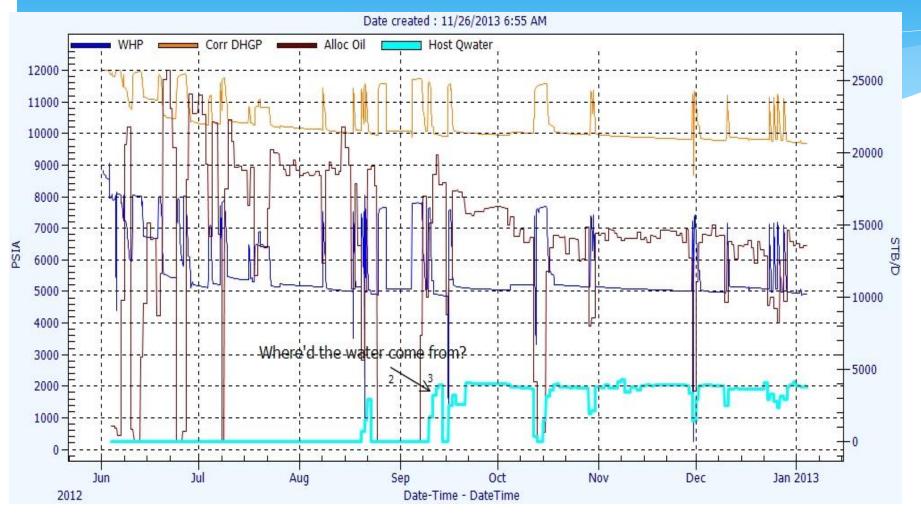
### Deepwater Oil Well (Water?)

 Start-up of New Deepwater Well (subsea)
 After just 3 months of Production, the well started making 4000 STB/D of WATER!

Objectives:

- 1) Find out where the water's coming from
- 2) See if it justifies a work-over

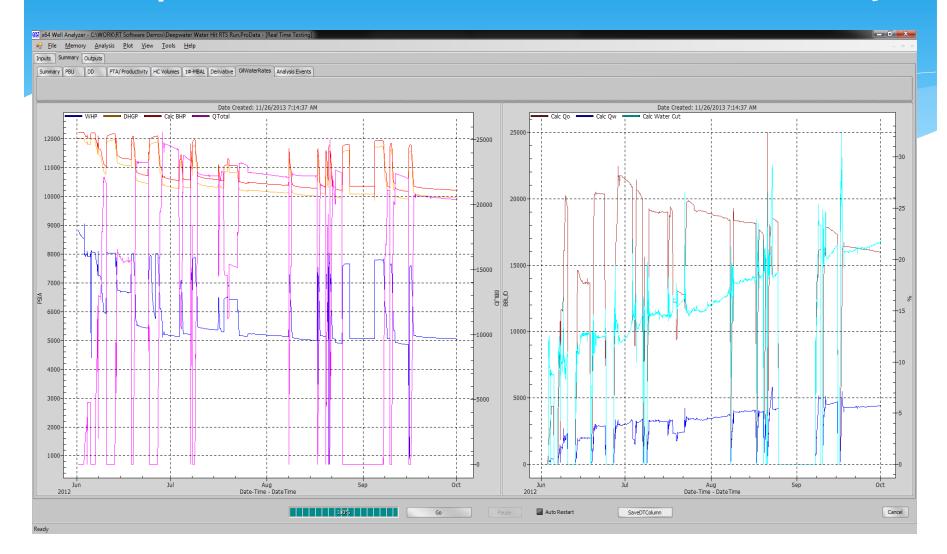
#### **Deepwater Oil – Allocated Rates**



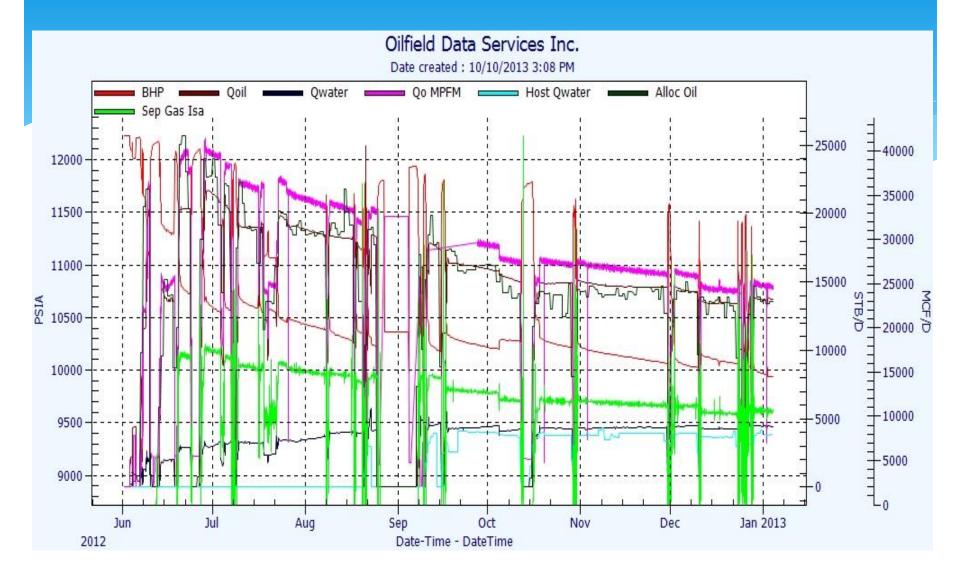
#### Deepwater Oil - WBS

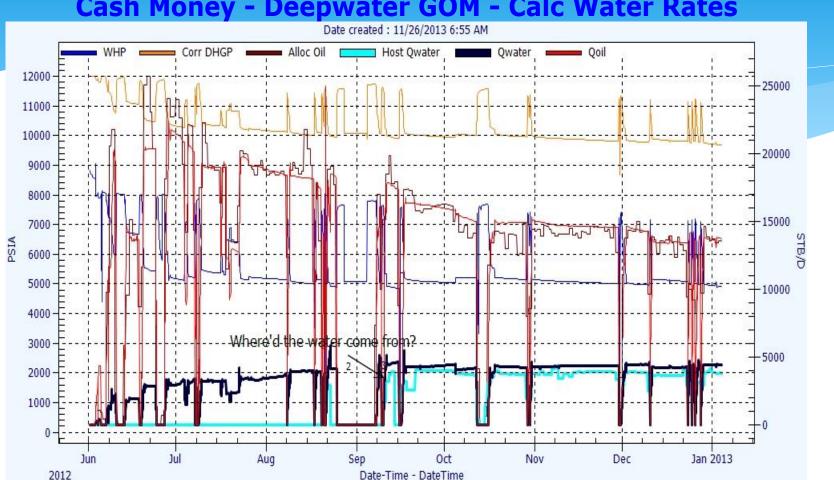
| Description   | Depth<br>(MD) | Depth<br>(TVD) | Length<br>(Pipe) | OD<br>(Pipe) | ID (Drift)     |  |
|---|---------------|----------------|------------------|--------------|----------------|--|
| (Deturn for measurements are from top)<br>Companys 15kms) Turbing Hanger  |               | (TVD)          | (Pipe)           |              |                |  |
| Cameron 15kpsi Tubing Hanger<br>Correction from E-Line to Production Tubing   | 6,503         | 6,503          | 1.13             | 17.305       | 4.607          |  |
| 5 1/2" 28.0# Vam Top HC Inc 13Cr/05 pup joint, PxP  | 6,508         | -              | 5.52             | 5.500        | 4.670          |  |
| 5 1/2" 28.0# Van Top HC Inc 13Cr/05 pup joint, BxP  | 6.512         | -              | 3.41             | 5.500        | 4.670          | 16" Rupture Disk @ 7,524' MD/TVD                               |
| 5 1/2" 28.0# VTKP x 23.0# VTHC 13Cr85 Timed pup joint, BxP  | 6,515         |                | 8.34             | 5.500        | 4.670          |  |
| 5 1/2" 23.0# Vam Top HC 13Cr 95 kal tubing, BxP   | 6,524         |                | 2,983.91         | 5.500        | 4.670          |  |
| 5 1/2" 23.0# Vam Top HC 13Cr 95 coupling, BxB   | 9,507         |                | 0.90             |              | 4.670          | SCSSV  |
| Methanol Inhibition mandrel 5-1/2" 23# Vam Top HC, PxP  | 9,508         | 9,508          | 5.94             |              | 4.560          | 16" Rupture Disk @ 9,010' MD/TVD                               |
| 5 1/2" 23.0# Vam Top HC 13Cr 95 Timed pup joint, BxP  | 9,514         |                | 6.43             | 5.500        | 4.670          | TOC @ 9,750' MD/TVD  |
| X-over, 5-1/2" 23# VTHC x 4-1/2" 15.1# Vem Top, 13Cr05, BxP   | 9,521         |                | 2.64             | 5.500        | 4.670          | 10 344" x 9 7/8" 10 718" MD/TVD                                |
| Plow Coupling, 4 1/2" 15.1# Vam Top 13Cr 95 BxB   | 9,523         |                | 6.52             |              | 3.798          |  |
| SCSSV, Neptune 4-1/2" 15.1# Vam Top, w/ 3.888" R nipple PxP           Prov Coupling, 4 1/2" 15.1# Vam Top 13Cr 95 BxP                                 | 9,530         | 9,529          | 14.39            | 7.400        | 3.688          | Completion Fluid   |
|   | 9,544         | <u> </u>       | 14.55            |              | 3.809          | Kill Weight Fluid: 12.8 ppg CeC                                |
| 4 1/2" 15.1# Vam Top 13Cr 95 pup joint, 8xP     4 1/2" 15.1# Vam Top 13Cr 95 tubing, 8xP  | 9,565         |                | 14.55            | 4.500        | 3.828          | Packer Fluid: 12.8 ppg CaCl.                                   |
| 5 4 1/2" 15 1# Vam Top 13Cr 95 public, 80   | 18,218        |                | 10.94            | 4.500        | 3.826          | w/Corrosion Inhibitor  |
| 18 DHPT Gauge Mandrel w/ Triple PQG gauges, PxP   | 18,228        | 18,169         | 8.15             | 7.451        | 3.760          | 16" Rupture Disk @ 11,018' MD/TVD                              |
| 17 4 1/2" 15 1# Vam Top 13Cr 95 Timed pup joint, BxB  | 18.237        |                | 8.92             | 4.500        | 3.789          | TOC @ 11,737 MD/TVD  |
| 18 DHPT Gauge Mandrel w/ Triple PQG gauges, PxP   | 18,248        | 18,185         | 8.15             | 7.451        | 3.760          |  |
| 9 4 1/2" 15.1# Vam Top 13Cr 95 Timed pup joint, BxB   | 18,254        |                | 6.93             | 4.500        | 3.828          | Control Lines  |
| 20 Deep Scale Inhibition Mandrel 4 1/2" 15.1# Vam Top, PxP  | 18,261        |                | 5.39             |              | 3,782          | (1) 30° Scale inhibitor line<br>(2) 14° SCSSV line             |
| 21 4 1/2" 15.1# Vam Top 13Cr 95 Timed pup joint, BxB  | 18,298        |                |                  | 4.500        |                | (1) 30" Asphaltene inhibitor in                                |
| 22 Deep Asphaltene Inhibition Mandrel 4 1/2* 15.1# Vam Top, PxP   | 18,273        | 18,210         | 5.39             | 6.398        | 3.762          | (2) 1/4" TEC lines<br>(1) 1/2" Methanol line                   |
| 23 4 1/2* 15.1# Vem Top 13Cr 95 pup joint, BxP  | 18,278        |                | 6.32             | 4.500        | 3.828          |  |
| 24 4 1/2" 15.1# Vem Top 13Cr 95 tubing, BxP (cut joint)   | 18,285        | <u> </u>       | 37.48            | 4.500        | 3.828          | TOC @ 12,303' MD/TVD   |
| 25 4 1/2" 15.1# Vam Top 13Cr 95 pup joint, BxP  | 18,322        | <u> </u>       | 10.30            | 4.500        | 3.828          | Production Tubing  |
| 28 Row Coupling, 4 1/2" 15.1# Vam Top 13Cr 85, BuP<br>77 "R" Landing Nimple, 4 1/2" 15.1# Vam Top 925, BvP  | 18,332        | 10.000         | 5.89             | 5.087        | 3.808          | 5-1/2* 23# 13Cr85 Vem Top                                      |
|   | 18,338        | 18,269         | 5.90             | 5.045        | 3.668          | ID 4.87", Dift 4.545" Coupling 4 1/2" 15 1# 13Cr85 Vam T       |
| 28 Flow Coupling, 4 1/2" 15.1# Vam Top 13Cr 85, BxP<br>29 4 1/2" 15.1# Vam Top 13Cr 95 pup joint, BxP   | 18,340        | <u> </u>       | 6.35             |              | 3.808          | 4 1/2" 15.1# 13Cr/6 Vam 1<br>ID 3.826" Drift 3.701" Coupling O |
| 20 4 1/2" 15.1# Vani Top 13Cr 95 pup joint, 60P<br>30 4 1/2" 15.1# Vani Top 13Cr 95 pup joint, 60P  | 18,340        | <u> </u>       | 10.21            |              | 3.789          | in a state still a store coupling o                            |
| 1 HNT Production Packer, 4 1/2" 15.1# Vam Top, BxP  | 18,362        | 18,291         | 10.37            | 8.303        | 3.788          |  |
| 22 Flow Coupling, 4 1/2" 15.1# Vem Top 13Cr 85, BxP   | 18.372        |                | 5.88             |              | 3,811          | KOP @ 16,763' MD (16,753' TVD)                                 |
| 33 "R" Landing Nipple, 4 1/2" 15.18 Alloy 725/120 Vam Top, BxP  | 18,378        | 18,305         | 1.30             | 5.042        | 3.688          |  |
| How Coupling, 4 1/2" 15.1# Vam Top 13Cr 85, BxP   | 18,380        |                | 5.88             | 5.084        | 3.811          |  |
| 35 4 1/2" 15.1# Vam Top 13Cr 95 perforated pup joint, BxP   | 18,385        |                | 6.32             | 4.500        | 3.794          | Production Casing  |
| 6 4 1/2" 15.1# Vam Top 13Cr 95 pup joint, BxP   | 18,392        |                | 10.33            | 4.500        | 3.789          | 10 3/4" 73.2# Q-125 HW-8T                                      |
| 7 X-over, 4 1/2" 15.1# Vam Top Pin x 6 5/8" 32# VTKP SC-80 Box  | 18,402        |                | 2.04             | 6.676        | 3.790          | ID 9.408", Dift 9.250"   |
| 85 8 5/8" 32# Vam Top KP SC-80, BxP, 13Cr85 tubing, LSOTJ   | 18,404        |                | 41.12            | 6.635        | 5.635          | 9 7/8" 62.8# HCQ-125 Vam Top<br>ID 8.625", Dift 8.500"         |
| 6 5/6" 32# Vem Top KP SC-80, BxP, 13Cr85 tubing, LSOTJ  | 18,445        |                | 81.53            | 6.635        | 5.635          |  |
| 43 6 5/8" 32# Vam Top KP SC-80, BxP, 13Cr85, pup joint, LSOTJ   | 18,527        | <u> </u>       | 10.43            | 6.635        | 5.635          |  |
| LSOTJ metered (Outer Upper Assembly)     LSOTJ metered (Outer Lower Assembly)   | 18,537        | <u> </u>       | 1.20             | 7.420        | 5.070          |  |
| <ol> <li>LSOTJ metered (Outer Lower Assembly)</li> <li>End of LSOTJ Assembly</li> </ol>   | 18,508        | <u> </u>       | 4.10             | 7.420        | 5.070          |  |
| 5 neck of telescoping assembly joint- Stroke begins   | 10,040        |                | 0.98             | 4.529        | 3.804          |  |
| 4 1/2" 15.1# Van FJL BrP, 13Cr95 production tubing  | 18,480        | -              | 82.10            | 4 520        | 3.804          |  |
| 7 4 1/2" 15 1# Vam FJL BaP, 13Cr95 production tubing  | 18.571        |                | 41.08            | 4.520        | 3.804          | - B  |
| 18 X-over pup, 4 1/2" 15.1# Vem FJL Box x Vem Top Pin, 13Cr95   | 18.612        |                | 9.88             | 4.529        | 3,804          |  |
| 4 1/2" 15.1# Vam Top 13Cr 95 pup joint, BxP   | 18,622        |                | 10.23            | 4.500        | 3.790          |  |
| 50 Flow Coupling, 4 1/2" 15.1# Vam Top 13Cr 85, BxP   | 18,632        |                | 5.89             | 5.042        | 3.798          |  |
| 1 "R" Landing Nipple, 4 1/2" 15.1# Alloy 725/120 Vam Top, BxP   | 18,638        | 18,541         | 1.20             | 5.060        | 3.688          |  |
| 2 Flow Coupling, 4 1/2" 15.1# Vem Top 13Cr 85, BxP  | 18,639        |                | 5.89             |              | 3.809          |  |
| 53 4 1/2" 15.1# Vam Top 13Cr 95 pup joint, BxP  | 18,645        | L              | 6.32             | 4.500        | 3.790          | LIOTA  |
| 54 4 1/2" 15.1# Vam Top 13Cr 95 pup joint, BxP  | 18,651        |                | 8.31             |              | 3.793          |  |
| 55 PFZ Ratchet latch Locator, 4 1/2" 15.1# Vam Top, 925<br>MSH Molded HNBR Seal Linit, 5 1/2" 20# Vam Top KP SC-80, ReP, 925                          | 18,660        | 18,561         | 2.06<br>6.26     | 6,819        | 3.793<br>4.783 |  |
| 56         MSH Molded HNBR Seal Unit, 5 1/2" 20# Vam Top KP SC-80, BxP, 925           57         Seal Extension, 5 1/2" 20# Vam Top KP SC-80 BxP, 925 | 18,002        |                | 8.04             | 5,980        | 4.763          | 3  |
| 57 Sear Extension, 5 172° 204 Vam Top KP SC-80 8xP, 925<br>58 MSH Molded HNBR Seal Unit, 5 1/2° 204 Vam Top KP SC-80, BaP, 925                        | 18,008        |                | 6.26             | 6.000        | 4.763          |  |
| 50 Seal Extension, 5 1/2" 20# Vam Top KP SC-80 BxP, 925   | 18,682        |                | 8.04             | 5.980        | 4.768          |  |
| 80 Sbg Self Aligning Mule Shoe, 5 1/2" 20# Vam Top KP SC-80 BM-, 925  | 18,690        |                | 3.51             | 5.946        | 4.766          |  |
| 1 End of Mule Shoe  | 18,694        |                |                  |              |                |  |
| 22 Completion Assembly  |               |                |                  |              |                |  |
| HES VCA Versa-Trieve 12.5k GP Packer, 718, HNBR   | 18,659        | 18,561         | 14.64            | 8.305        | 6.000          |  |
| HES Circ. Housing w/ MCS closure sleeve   | 18,674        |                | 6.48             | 8.300        | 6.000          |  |
| 5 X-over, 7 5/8" 42.8# AB-HDL Box x 5 1/2" 23# Vam Top HC Pin, 925  | 18,681        |                | 25.08            |              | 6.010          |  |
| 8 5 1/2" 23# Vem Top HC BxP Make-up sub, Inc 925  | 18,708        |                | 3.58             | 7.247        | 4.590          |  |
| 5 1/2" 23# Vam Top HC BxP pup joint, 13Cr85   | 18,709        |                | 4.18             | 5.508        | 4.589          |  |
| 5 1/2" 23# Vam Top HC BxP pup joint, 13Cr85   | 18,713        |                | 8.42             | 5.508        | 4.589          |  |
| FS-2 Formation Isolation Valve 5 1/2" 23# Inc 718 Vam Top HC  | 18,722        | 18,617         | 17.00            | 8.010        | 3.870          |  |
| 0 51/2" 23# Vem Top HC BxP pup joint, 13Cr85  | 18,739        | <u> </u>       |                  | 5.508        | 4.589          |  |
|   | 18,745        | I              | 8.34             | 5.508        | 4.597          |  |
| 72 5 1/2" 23# Vam Top HC, MJS. Shear Sub, (90K shear), Inc 925 BoP  | 18,754        | <u> </u>       | 8.35             |              | 4.612          |  |
| 73 5 1/2" 23# Van Top HC BxP pup joint, 13Cr85  | 18,758        | <u> </u>       |                  | 5.508        |                |  |
| 74 5 1/2" 23# 13Cr85 Vam Top HC Blank Pipe w/ Centralizers<br>75 5 1/2" 23# 13Cr85 Vam Top HC Premium Screen 175 mesh                                 | 18,763        | <u> </u>       | 88.98            |              | 4.612          |  |
| 6 Top Snap, 51/2" 23# Vam Top HC Premum Screen 1/5 meen<br>76 Top Snap, 51/2" 23# Vam Top HC Box x 17# Vam Top SC80 Pin                               | 18,970        | 18.842         | 120.40           | 8,185        | 4.512          |  |
| 77 HMBR Seal assembly w/ self aligning shoe 190/80  | 18.971        | -              | 42.84            | 5.950        | 4.875          |  |
| 7 PMbh Seal assembly wriser aigning shoe 130/80<br>78 End of Guide Shoe   | 19,014        |                | 74.04            | 0.450        | 4.070          |  |
| Per character character character   | 10000         |                |                  | <u> </u>     | <u> </u>       | 45340 200004 20  |
| 30 Sump Packer Assembly (Wireline Set)  |               |                |                  |              |                | のないので  |
| Sump Packer, (HMBR) w/ mule shoe  | 18,970        | 18,842         | 6.77             | 8.310        | 6.000          | RA Tag —   |
| 2 Bottom of Packer  | 18,977        |                |                  |              |                |  |
| 1   |               |                |                  |              |                | <b>新新市会社</b>   |
|   |               | 18,942         |                  |              |                |  |
| 34 Steel Bridge Plug  | 19,080        |                |                  |              |                |  |
|   |               | 18,957         |                  |              | 17200          | TS Hope  |

#### Deepwater Oil – Calc Rates Summary



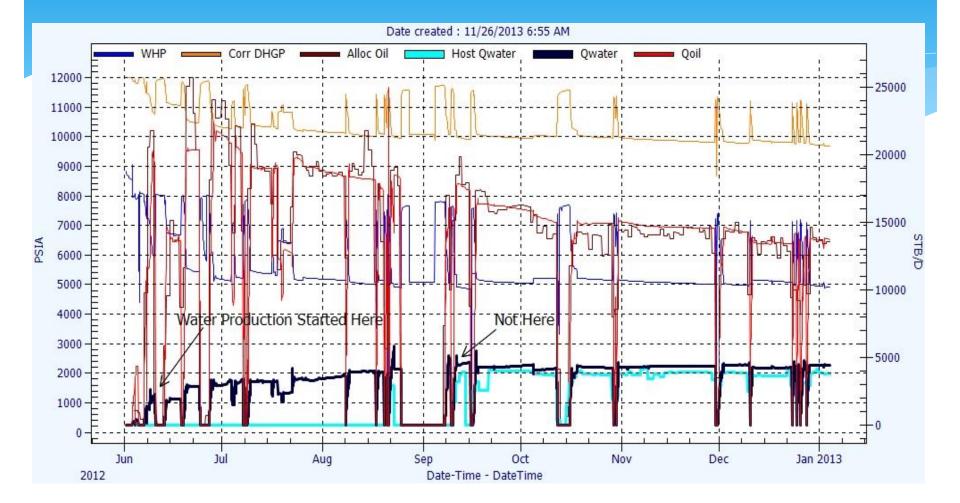
#### **Cash Money #2 - Deepwater Rates & BHPs**





#### **Cash Money - Deepwater GOM - Calc Water Rates**

#### When did the Water Production Begin???



151

# YES... ALLOCATIONS REALLY ARE THIS BAD!!

#### Deepwater Oil – RTS Summary

|         | ry Outputs                      |                               |                         |              |              |              |               |               |              |              |                 |               |                            |   |               |               |             |                  |                       |                       |       |
|---------|---------------------------------|-------------------------------|-------------------------|--------------|--------------|--------------|---------------|---------------|--------------|--------------|-----------------|---------------|----------------------------|---|---------------|---------------|-------------|------------------|-----------------------|-----------------------|-------|
| y       | PBU DD PTA/P                    | roductivity HC Volumes 1Φ-    | MBAL Deriv              | ative OilWa  | terRates A   | nalysis Even | its           |               |              |              |                 |               |                            |   |               |               |             |                  |                       |                       |       |
|         | Start D/T<br>ddMmmyyyy hh:mm:ss | End D/T<br>ddMmmyyyy hh:mm:ss | Test<br>Length<br>Hours | Test<br>Type | WHPi<br>psia | WHPf<br>psia | DHGPi<br>psia | DHGPf<br>psia | BHPi<br>psia | BHPf<br>psia | Qoil_i<br>BBL/D | Qoil<br>BBL/D | Perm<br>md                 | Skin  | DPskin<br>psi | PStar<br>psia | PI Eff<br>% | DPs/Q<br>psi/BBL | Report Link           | Graph Link            |       |
|         | 05Jun2012 10:24:00              | 06Jun2012 22:56:00            | 36.53                   | PBU          | 7915         | 8063         | 11803         | 12011         | 12010        | 12221        | 4380            | 4380          | 447.2                      | 0.8   | 21            | 12241         | 88          | 0                | RTRep 2012Jun05 10240 | RTRep 2012Jun05 10240 |       |
|         | 10Jun2012 10:44:00              | 13Jun2012 07:11:00            | 68.45                   | PBU          | 5923         | 8032         | 10769         | 11973         | 11027        | 12183        | 19303           | 19303         | 486                        | 3.3   | 335           | 12283         | 65          | 0.02             | RTRep 2012Jun10 10440 | RTRep 2012Jun10 10440 |       |
|         | 18Jun2012 13:05:00              | 19Jun2012 04:11:00            | 15.1                    | PBU          | 6665         | 8032         | 11058         | 11890         | 11293        | 12095        | 13665           | 13665         | 244.2                      | -1.6  | -220          | 12271         | 135         | -0.02            | RTRep 2012Jun18 13050 | RTRep 2012Jun18 13050 |       |
|         | 19Jun2012 04:11:00              | 24Jun2012 07:37:00            | 123.43                  | DD           | 8030         | 7188         | 11888         | 11290         | 12094        | 11509        | 0               | 20300         | 106.1                      | -4.6  | -2191         | 10558         | 582         | -0.11            | RTRep 2012Jun19 04110 | RTRep 2012Jun19 04110 |       |
|         | 24Jun2012 07:37:00              | 27Jun2012 00:33:00            | 64.93                   | PBU          | 7189         | 8021         | 11290         | 11898         | 11509        | 12105        | 9070            | 9070          | 358.4                      | 0.6   | 39            | 12245         | 91          | 0                | RTRep 2012Jun24 07370 | RTRep 2012Jun24 07370 |       |
|         | 27Jun2012 00:33:00              | 03Jul2012 20:48:00            | 164.25                  | DD           | 8021         | 5126         | 11898         | 10273         | 12105        | 10547        | 0               | 17402         | 48.2                       | -5.6  | -5243         | 10385         | 1389        | -0.3             | RTRep 2012Jun27 00330 |                       |       |
|         | 08Jul2012 03:20:00              | 08Jul2012 23:54:00            | 20.57                   | PBU          | 6089         | 7917         | 10711         | 11777         | 10957        | 11983        | 15631           | 15631         | 522.6                      | 5.6   | 426           | 12145         | 53          | 0.03             | RTRep 2012Jul08 03200 | RTRep 2012Jul08 03200 |       |
|         | 08Jul2012 23:54:00              | 16Jul2012 10:05:00            | 178.18                  | DD           | 7916         | 5365         | 11776         | 10320         | 11982        | 10584        | 0               | 19148         | 311.8                      | 0.8   | 125           | 10497         | 88          | 0.01             | RTRep 2012Jul08 23540 | RTRep 2012Jul08 23540 |       |
|         | 20Aug2012 19:59:30              | 21Aug2012 07:59:30            | 12                      | PBU          | 5533         | 7700         | 10306         | 11589         | 10560        | 11796        | 15579           | 15579         | 241.4                      | 0.4   | 63            | 12034         | 94          | 0                | RTRep 2012Auq20 19593 |                       |       |
| ļ       | 21Aug2012 10:33:30              | 25Aug2012 06:29:30            | 91.93                   | 2-Rate       | 7255         | 4891         | 11296         | 9939          | 11511        | 10208        | 3207            | 13735         | 231.6                      | 0.5   | 77            | 11280         | 92          | 0.01             | RTRep 2012Aug21 10333 |                       |       |
|         | 25Aug2012 06:29:30              | 07Sep2012 13:14:30            | 318.75                  | PBU          | 4894         | 7805         | 9940          | 11731         | 10209        | 11940        | 18213           | 18213         | 614.6                      | 13  | 981           | 11996         | 33          | 0.05             | RTRep 2012Aug25 06293 | RTRep 2012Aug25 06293 |       |
|         | 09Sep2012 15:10:30              | 10Sep2012 04:08:30            | 12.97                   | PBU          | 5043         | 7635         | 10044         | 11652         | 10310        | 11867        | 16157           | 16157         | 589.8                      | 14.2  | 1008          | 12028         | 31          | 0.06             | RTRep 2012Sep09 15103 |                       |       |
|         |                                 | **** *********                | ~7 40                   |              |              | E100         | 11000         | 10001         | 11001        | 10000        | ^               | 15000         | 100 1                      | ~ 7   |               | 0001          | 100         | 0 0F             | DTDop 2012Cop10 04002 |                       |       |
|         |                                 |                               |                         |              |              |              |               |               |              |              |                 |               | -25000                     | 12000   | Ei            | KA.           | AF          |                  | К.,                   |                       | FIN A |
|         |                                 |                               |                         |              |              |              |               |               |              |              |                 |               | -20000                     | 12000<br>11000<br>10000<br>9000<br>8000                               |               |               |             |                  |                       |                       |       |
| ))))))) |                                 |                               |                         |              |              |              |               |               |              |              |                 |               |                            | 11000<br>10000<br>9000<br>8000<br>7000<br>6000                        |               |               |             |                  |                       |                       |       |
|         |                                 |                               |                         |              |              |              |               |               |              |              |                 |               | -20000<br>-15000<br>-10000 | 11000<br>9000<br>8000<br>7000<br>6000<br>5000<br>4000                 |               |               |             |                  |                       |                       |       |
|         |                                 |                               |                         |              |              |              |               |               |              |              |                 |               | -20000<br>-15000           | 11000<br>9000<br>8000<br>7000<br>6000<br>5000<br>4000<br>3000<br>2000 |               |               |             |                  |                       |                       |       |
|         |                                 |                               |                         |              |              |              |               |               |              |              |                 |               | -20000<br>-15000<br>-10000 | 11000<br>9000<br>8000<br>5000<br>5000<br>4000<br>3000                 |               |               |             |                  |                       |                       |       |
| 0-      |                                 |                               |                         | Sat          |              |              |               |               |              |              |                 |               | -20000<br>-15000<br>-10000 | 11000<br>9000<br>8000<br>7000<br>6000<br>5000<br>4000<br>3000<br>2000 |               |               |             |                  |                       |                       |       |

#### **Deepwater Oil – PBU Summary**

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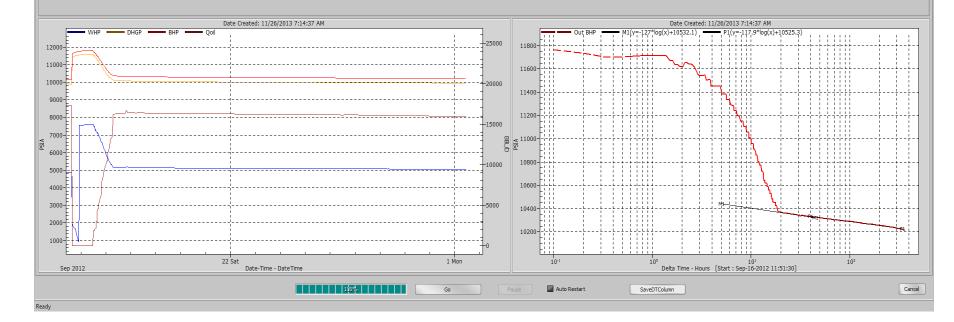
#### 🥨 x64 Well Analyzer - C:\WORK\RT Software Demos\Deepwater Water Hit RTS Run.ProData - [Real Time Testing

🖳 File Memory Analysis Plot View Tools Help

Inputs Summary Outputs

Summary PBU DD PTA/Productivity HC Volumes 10-MBAL Derivative OlWaterRates Analysis Events

|   | Start D/T<br>ddMmmyyyy hh:mm:ss | End D/T<br>ddMmmyyyy hh:mm:ss | Test<br>Length<br>Hours | Test<br>Type | WHPi<br>psia | WHPf<br>psia | DHGPi<br>psia | DHGPf<br>psia | BHPi<br>psia | BHPf<br>psia | Qoil_i<br>BBL/D | Qoil<br>BBL/D | Perm<br>md | Skin | DPskin<br>psi | PStar<br>psia | PI Eff<br>% | DPs/Q<br>psi/BBL | Report Link           | Graph Link            |
|---|---------------------------------|-------------------------------|-------------------------|--------------|--------------|--------------|---------------|---------------|--------------|--------------|-----------------|---------------|------------|------|---------------|---------------|-------------|------------------|-----------------------|-----------------------|
| 1 | 05Jun2012 10:24:00              | 06Jun2012 22:56:00            | 36.53                   | PBU          | 7915         | 8063         | 11803         | 12011         | 12010        | 12221        | 4380            | 4380          | 447.2      | 0.8  | 21            | 12241         | 88          | 0                | RTRep 2012Jun05 10240 | RTRep 2012Jun05 10240 |
| 2 | 10Jun2012 10:44:00              | 13Jun2012 07:11:00            | 68.45                   | PBU          | 5923         | 8032         | 10769         | 11973         | 11027        | 12183        | 19303           | 19303         | 486        | 3.3  | 335           | 12283         | 65          | 0.02             | RTRep 2012Jun10 10440 | RTRep 2012Jun10 10440 |
| 3 | 18Jun2012 13:05:00              | 19Jun2012 04:11:00            | 15.1                    | PBU          | 6665         | 8032         | 11058         | 11890         | 11293        | 12095        | 13665           | 13665         | 244.2      | -1.6 | -220          | 12271         | 135         | -0.02            | RTRep 2012Jun18 13050 | RTRep 2012Jun18 13050 |
| 4 | 24Jun2012 07:37:00              | 27Jun2012 00:33:00            | 64.93                   | PBU          | 7189         | 8021         | 11290         | 11898         | 11509        | 12105        | 9070            | 9070          | 358.4      | 0.6  | 39            | 12245         | 91          | 0                | RTRep 2012Jun24 07370 | RTRep 2012Jun24 07370 |
| 5 | 08Jul2012 03:20:00              | 08Jul2012 23:54:00            | 20.57                   | PBU          | 6089         | 7917         | 10711         | 11777         | 10957        | 11983        | 15631           | 15631         | 522.6      | 5.6  | 426           | 12145         | 53          | 0.03             | RTRep 2012Julo8 03200 | RTRep 2012Julo8 03200 |
| 6 | 20Aug2012 19:59:30              | 21Aug2012 07:59:30            | 12                      | PBU          | 5533         | 7700         | 10306         | 11589         | 10560        | 11796        | 15579           | 15579         | 241.4      | 0.4  | 63            | 12034         | 94          | 0                | RTRep 2012Auq20 19593 | RTRep 2012Auq20 19593 |
| 7 | 25Aug2012 06:29:30              | 07Sep2012 13:14:30            | 318.75                  | PBU          | 4894         | 7805         | 9940          | 11731         | 10209        | 11940        | 18213           | 18213         | 614.6      | 13   | 981           | 11996         | 33          | 0.05             | RTRep 2012Aug25 06293 | RTRep 2012Aug25 06293 |
| 8 | 09Sep2012 15:10:30              | 10Sep2012 04:08:30            | 12.97                   | PBU          | 5043         | 7635         | 10044         | 11652         | 10310        | 11867        | 16157           | 16157         | 589.8      | 14.2 | 1008          | 12028         | 31          | 0.06             | RTRep 20125ep09 15103 | RTRep 20125ep09 15103 |
| 9 | 15Sep2012 15:23:30              | 16Sep2012 11:51:30            | 20.47                   | PBU          | 4852         | 7608         | 9903          | 11605         | 10172        | 11818        | 17270           | 17270         | 389.6      | 6.8  | 774           | 12005         | 48          | 0.04             | RTRep 2012Sep15 15233 | RTRep 2012Sep15 15233 |



#### Deepwater Oil – DD Summary

|    | Summary Outputs                 |  |                         |              |              |              |                |                |                |                |                 |               |            |         |                      |                |             |                  |                           |   |                                       |     |
|----|---------------------------------|--|-------------------------|--------------|--------------|--------------|----------------|----------------|----------------|----------------|-----------------|---------------|------------|---------|----------------------|----------------|-------------|------------------|---------------------------|---|---------------------------------------|-----|
| )  | y PBU DD PTA/F                  | Productivity HC Volumes 10               | -MBAL Deri              | vative OilWa | aterRates    | Analysis Ev  | ents           |                |                |                |                 |               |            |         |                      |                |             |                  |                           |   |                                       |     |
|    | Start D/T<br>ddMmmyyyy hh:mm:ss | End D/T<br>ddMmmyyyy hh:mm:ss            | Test<br>Length<br>Hours | Test<br>Type | WHPi<br>psia | WHPf<br>psia | DHGPi<br>psia  | DHGPf<br>psia  | BHPi<br>psia   | BHPf<br>psia   | Qoil_i<br>BBL/D | Qoil<br>BBL/D | Perm<br>md | Skin    | DPskin<br>psi        | PStar<br>psia  | PI Eff<br>% | DPs/Q<br>psi/BBL | Report Link               | Graph Link  |                                       |     |
|    |                                 | 24Jun2012 07:37:00<br>03Jul2012 20:48:00 |                         | DD<br>DD     | 8030<br>8021 | 7188<br>5126 | 11888<br>11898 | 11290<br>10273 | 12094<br>12105 | 11509<br>10547 |                 | 20300         |            |         |                      | 10558<br>10385 | 582<br>1389 |                  | RTRep 2012Jun19 04110     | RTRep 2012Jun19 04110<br>0 US DD inc<br>RTRep 2012Jun27 00330 |                                       |     |
|    | 08Jul2012 23:54:00              | <u></u>                                  |                         |              | 7916         | 5365         |                |                | 11982          |                |                 | 19148         |            | 0.8     |                      | 10497          | 88          |                  | RTRep 2012Jul08 23540     | O LIC DD CDD ing  |                                       |     |
|    | 21Aug2012 10:33:30              | 25Aug2012 06:29:30                       | 91.93                   | 2-Rate       | 7255         | 4891         | 11296          | 9939           | 11511          | 10208          | 3207            | 13735         | 231.6      | 0.5     | 77                   | 11280          | 92          |                  | RTRep 2012Aug21 10333     | RTRep 2012Aug21 10333   |                                       |     |
|    |                                 | 11Sep2012 07:33:30                       |                         |              | 7671         |              | 11652          |                | 11864          | 10360          |                 | 15836         |            | -2.7    |                      | 9881           | 188         |                  |                           | RTRep 20125ep10 04083   |                                       |     |
|    | 16Sep2012 11:51:30              | 01Oct2012 11:18:30                       | 359.45                  | DD           | 7608         | 5048         | 11605          | 9953           | 11818          | 10215          | 0               | 16325         | 358.8      | 5.4     | 600                  | 10172          | 53          | 0.04             | RTRep 20125ep16 11513     | RTRep 20125ep16 11513   |                                       |     |
|    |                                 |  |                         | Date Created | d: 11/26/2   | 013 7:14:    | 37 AM          |                |                |                |                 |               |            |         |                      |                |             |                  |                           | 26/2013 7:14:37 AM  |                                       |     |
|    | E                               | DHGP BHP                                 | - Qoil                  | 1            |              |              |                |                |                |                |                 | 1             |            |         |                      | - Out Bi       | IP          | 1 1 1 1          | 11 1 1 1                  | P1(y=-117.9*log(x)+10525.                                     |                                       |     |
| ſ  |                                 |  |                         |              |              |              |                |                |                |                |                 |               |            | 11800   |                      |                |             | + - +            | 11 1 1 1                  | -ll- + -l-ll<br>  |                                       | ++- |
| )( | 0-E\ <del>\</del>               |  |                         |              |              |              |                |                |                |                |                 |               | -          | 11600   |                      |                |             |                  |                           |   |                                       |     |
| )( | , []                            |  |                         |              |              |              |                |                |                |                |                 | <u></u>       |            |         |                      |                |             |                  | 11 I I I <b>1</b> 1       |   |                                       |     |
|    | E                               |  |                         |              |              |              |                |                |                |                |                 |               | -20000     | 11400   | -     <br> - -¦-¦-¦- |                |             |                  | ++++++++++++++            | <b>↓</b> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,                 |                                       |     |
| )( |                                 |  |                         |              |              |              |                |                |                |                |                 |               |            |         | Ett                  |                |             | 1 1 1 1          | 11 1 1 1                  | 1 <b>%</b> [::::  |                                       |     |
| )( | ر <u>س</u> ے                    |  |                         |              |              |              |                |                |                |                |                 |               |            | 11200   | ┝┥╬╸╠╠╸╺╵<br>┍╷╷╷╷   |                | ++-         | • + - + - + - +  | ++++++++++++++            |   |                                       |     |
| )( | ,EL                             |  |                         |              |              |              |                |                |                |                |                 |               | -15000     |         |                      |                |             | 1 1 1 1          |                           | 111 <b>1</b>  |                                       |     |
|    | EL \                            |  |                         |              |              |              |                |                |                |                |                 |               |            | 11000 A |                      |                |             | 1111             |                           | ····  |                                       |     |
|    | ⁰==\                            |  |                         |              |              |              |                |                |                |                |                 |               | -          | 10800   | Ett.                 |                |             |                  | 11 1 1 1                  | <b>\</b>  | · · · · · · · · · · · · · · · · · · · |     |
| )( | ₀┋┼╌╌╌┼╌╌╌╴                     |  |                         |              |              |              |                |                |                |                |                 |               | +10000     | 10000   |                      |                |             |                  | 11 1 1 1                  |   |                                       |     |
|    | . El                            |  |                         |              |              |              |                |                |                |                |                 |               | -          | 10600   | -i i i<br>           |                |             | +-+-+            | +++++                     | <b>-</b>  |                                       |     |
| 00 | EL /                            |  |                         |              |              |              |                |                |                |                |                 |               | -          |         | E                    |                |             |                  |                           | 111111 1  |                                       |     |
| 00 | 0                               |  |                         |              |              |              |                |                |                |                |                 |               | -5000      | 10400   | ┥┥┾┝╺╶               |                |             | · + - +          | +++++++++++++-            | M <u>h-1</u> _1_1_1_<br>                                      |                                       |     |
| 00 | 0-E                             |  |                         | ·+           |              |              |                |                |                |                |                 | ·             | -          |         |                      |                |             |                  |                           |   | T                                     |     |
|    | YENE J                          |  |                         |              |              |              |                |                |                |                |                 |               | 1          | 10200   | )                    |                |             | • + - + +        | ii i i i                  |   | · · · · · · · · · · · · · · · · · · · |     |
|    | ENY                             |  |                         | 1            |              |              |                |                |                |                |                 | 1             | -0         |         |                      |                |             |                  |                           |   |                                       |     |
|    |                                 |  |                         |              |              |              |                |                |                |                | 1               |               | 1          |         |                      |                |             |                  |                           |   |                                       |     |
|    | ENY                             | · · · ·                                  | 2                       | 2 Sat        | e-Time - Da  | toTime       |                |                |                |                | 1               | Mon           | <u>ц</u>   |         | 10'1                 |                |             |                  | 10°<br>Data Tima Hours II | 10 <sup>1</sup><br>Start : Sep-16-2012 11:51:30]              | 10 <sup>2</sup>                       |     |

#### \* How Much Oil Should it Produce?

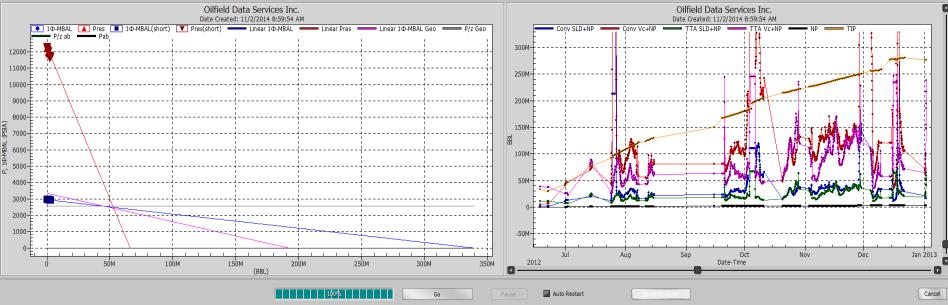
#### 🗱 x64ODSI-Well Analyzer - C:\WORK\RT Software Demos\Deepwater Water Hit RTS Run.ProData - [Real Time Testing]

<u>File Memory Analysis Plot View Tools Help</u>

| Inputs | Summary | Outputs |  |
|--------|---------|---------|--|
|--------|---------|---------|--|

#### Summary PBU DD PTA/Productivity HC Volumes 10-MBAL Derivative OilWaterRates Analysis Events

| Date Time           | Oil<br>Produced | PBU<br>Duration | Pres  | z-Factor | 1Φ-<br>MBAL | GIP SLD @P=0 | GIP SLD<br>@P ab= | GIP 1Φ-MBAL<br>@P=0 | GIP 1Φ-MBAL<br>@ab=NaN | GIP 1Φ-MBAL<br>geo @P=0 | GIP 1Φ-MBAL<br>geo @ab=NaN | m Pres     | m 1Φ-MBAL  | m 1Φ-<br>MBAL G |
|---------------------|-----------------|-----------------|-------|----------|-------------|--------------|-------------------|---------------------|------------------------|-------------------------|----------------------------|------------|------------|-----------------|
| MM/dd/yyyy HH:mm:ss | MMBBL           | HOURS           | PSIA  | dimless  | PSIA        | MMBBL        | MMBBL             | MMBBL               | MMBBL                  | MMBBL                   | MMBBL                      | PSIA/MMBBL | PSIA/MMBBL | PSIA/M          |
| 01/01/0001 00:00:0  | 0.000           |                 | 12232 | 4.145    | 2950.8      |              |                   |                     |                        |                         |                            |            |            |                 |
| 06/06/2012 22:56:00 | 0.007           | 37              | 12241 | 4.148    | 2951.21     |              |                   |                     |                        |                         |                            |            |            |                 |
| 06/13/2012 07:11:00 | 0.053           | 68              | 12283 | 4.159    | 2953.16     |              |                   |                     |                        |                         |                            |            |            |                 |
| 06/19/2012 04:11:00 | 0.122           | 15              | 12271 | 4.156    | 2952.60     |              |                   |                     |                        |                         |                            |            |            |                 |
| 06/27/2012 00:33:00 | 0.214           | 65              | 12245 | 4.149    | 2951.39     |              |                   |                     |                        |                         |                            |            |            |                 |
| 07/08/2012 23:54:00 | 0.421           | 21              | 12145 | 4.121    | 2946.75     |              |                   |                     |                        |                         |                            |            |            |                 |
| 08/21/2012 07:59:30 | 1.160           | 12              | 12034 | 4.091    | 2941.56     |              |                   |                     |                        |                         |                            |            |            |                 |
| 09/07/2012 13:14:3  | 1.223           | 319             | 11996 | 4.081    | 2939.7      | 63.4         | 63.4              | 326.8               |                        | 185.1                   |                            | -192.9     | -9.0       | -18.1           |
| 09/10/2012 04:08:30 | 1.252           | 13              | 12028 | 4.089    | 2941.26     | 63.4         | 63.4              | 326.8               |                        | 185.1                   |                            | -192.9     | -9.0       | -18.1           |
| 09/16/2012 11:51:30 | 1.343           | 20              | 12005 | 4.083    | 2940.18     | 63.4         | 63.4              | 326.8               |                        | 185.1                   |                            | -192.9     | -9.0       | -18.1           |
| 10/16/2012 00:48:3  | 1.745           | 89              | 11912 | 4.058    | 2935.8      | 66.2         | 66.2              | 340.2               |                        | 192.6                   |                            | -184.8     | -8.7       | -17.3           |



#### Deepwater Oil - Conclusions

- Err... no need to panic, it's been making water since
   Day One
- \* Min In-place oil = 65 MM STB
- \* Max In-place oil = 260 MM STB
- \* Min recoverable oil = 40-ish MM STB
- Enough Oil to justify work-over... but, the well doesn't need a work-over

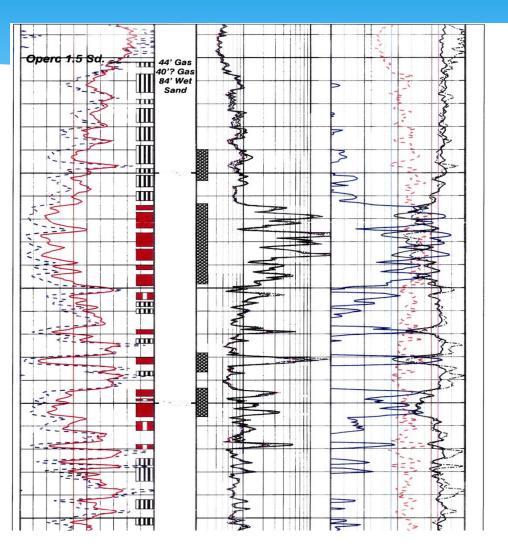
#### Deep GOM Shelf – Gas/Condensate

- \* 18,000 psia Pinitial; 330 degF
- \* Initial Flowback 20 MMscf/D; 400 BOPD
- \* Objectives:
  - \* Can we pull it harder?
  - \* How big is it?
  - \* No, really... how big is it? How much is water?
  - \* What's up with the perms being all over the place?

### **GOM Shelf IPT**

- Gulf Of Mexico Gas Condensate Well
- Has SCADA WHP Gauge + Instant Separator Gas and Periodic Liquid Rates
- Have To Apply Liquid Residence Time (Else Turbine Meter Data Would Result In High Or Low Rates Due To Separator Dumps)
- Objectives:
  - Calculate Liquid Rates
  - Analyze Build-up Tests
  - Split Apparent Reserves into Components

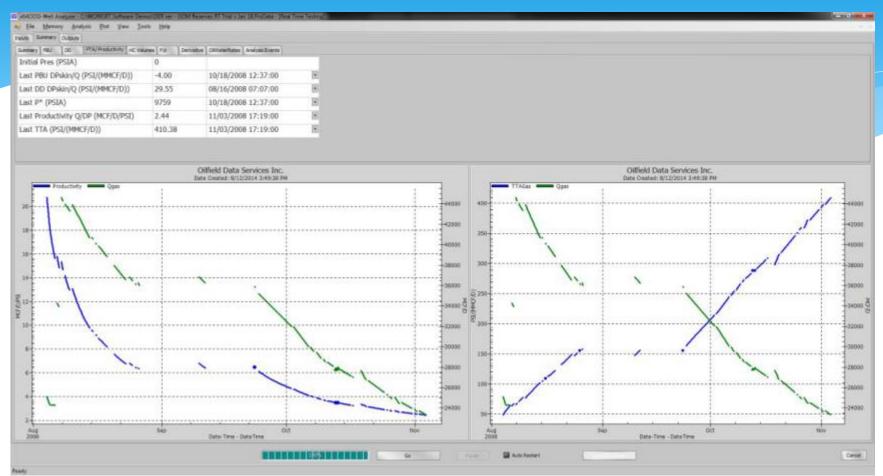
# Logs – GOM Shelf



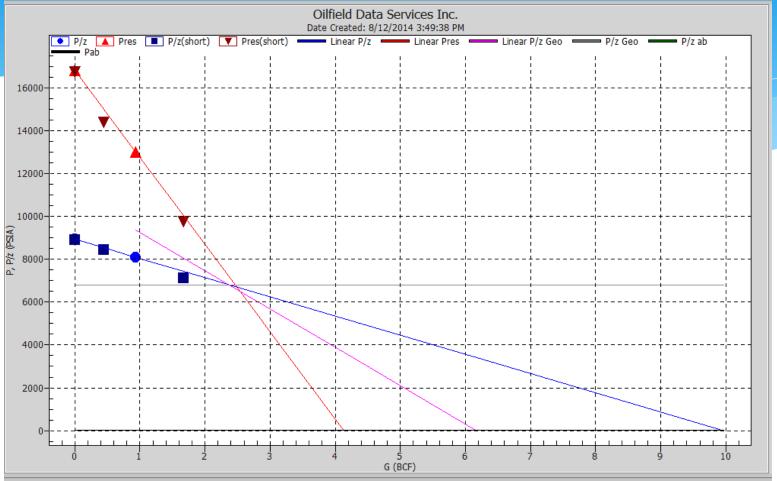
#### **GOM Shelf IPT**

| ۰. | Marriery Analysis I  | Dat Yew Justs Helt                       |                         |              |               |                |               |                  |                |              |                |                    |            |             |               |                |           |  |  |  |        |     |
|----|--|--|-------------------------|--------------|---------------|----------------|---------------|------------------|----------------|--------------|----------------|--------------------|------------|-------------|---------------|----------------|-----------|--|--|--|--------|-----|
| 3  | unmary Outpate   |  |                         |              |               |                |               |                  |                |              |                |                    |            |             |               |                |           |  |  |  |        |     |
| -  | 78U 00 F7A/R   | nductody   +C values   P/r               | Dense                   | the Oliviati | eRates A      | wirst Event    | 1             |                  |                |              |                |                    |            |             |               |                |           |  |  |  |        |     |
|    | Start D/T<br>MPInumynyy Normerse   | End D/T<br>ddHanegyyy blczaraces         | Test<br>Longth<br>Hours | Tast<br>Type | WEEN puts     | weard<br>pain  | DHGP1<br>pein | Designet<br>gaaa | Really<br>pade | anat<br>prin | QGasi<br>Mcf/D | QGas<br>Pict/D     | Pares      | Shin        | DPskan<br>pri | Pillar<br>pens | -         | DiPu/10<br>post/PRPsed   | Report Link                                | Graph Link                               |        |     |
|    | And the second sec | 03Aug2008 04:19:00<br>15Aug2008 16:49:00 | 8.4<br>7.2              | 0D<br>PBU    | 13876<br>8642 | 13239<br>11313 | -1            | 4                | 16720          | 16174        | 0 40554        | 15300              | 9.1<br>16  | -1.9<br>1.3 |               | 15899<br>14374 | 150<br>83 | -14.98   | ODSIRTERS 2008Aug62<br>DOSIRTERS 2008Aug15 | ODSINTREP 2508Aug02<br>UNITREP 2508Aug02 |        |     |
|    | the second second second second second second second second second second second second second second second se  | 225ep2008 17:01:00                       | 267.2                   | PBU          | 7505          | 10128          | -1            | -4               | 11115          | 1000000      | 36203          | Contraction of the | 20.1       | 2.3         |               | 13009          | 72        | the second second second second second second second second second second second second second second second s | ODSIRTRes 20085en11                        | AND A REAL FOR ADDITIONAL                |        |     |
|    | 170ct2008 03:43:00   | 180ct2006 12:37:00                       | 32.9                    | PBU          | 5448          | 7046           | -1            | -1               | 8429           | 9292         | 26998          | 26998              | 12.9       | -0.8        | -105          | 9759           | 116       | -4   | 0053879au 20100:117 8                      | ODERTRes 20090x117                       | 2      |     |
|    |  |  |                         | Olfield      | Data Se       | wices In       | с.            |                  |                |              |                |                    |            |             |               |                |           |  | Offield Data                               | Services Inc.                            |        |     |
|    |  |  |                         | late Cinitie |               |                |               |                  |                |              |                |                    |            |             | _             |                |           |  | Date Orested: 8/12                         |  |        |     |
|    | -  | an (\$90                                 |                         |              |               |                |               |                  |                |              |                |                    | 45000      | 26000       | 1             | m              |           | Qpa  |  |  |        | -T- |
| 0  | È  |  |                         |              |               |                |               |                  |                |              |                |                    | 40096      | 14000       |               |                | D         |  |  |  |        | 1   |
|    | ļ  |  |                         |              |               |                |               |                  |                |              |                |                    | 35000      | 12900       | EIL.          |                |           | 11-  |  | -  |        | -   |
|    | -  |  |                         |              |               |                |               |                  |                |              |                |                    | 30078      | 10000       | E             |                |           |  |  | KI                                       | These  | 1   |
|    | L  |  |                         |              |               | n -            |               |                  |                | 1            |                | Т                  | 23008<br>g |             | EIN           | T              | 4         |  |  |  | HUT    |     |
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| 10 |  |  |                         |              | -             | -              |               |                  |                |              |                |                    | 15008      | 4000        |               |                |           |  |  |  | 11-11- | T   |
|    | Ē  |  |                         |              |               |                |               |                  |                |              |                |                    | 10000      | 2000        |               |                |           |  |  |  |        |     |
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| 10 | L  | 32 We                                    |                         |              | - Term - Da   | tu Time        | ***           |                  | 1              | Set.         |                |                    | 1          |             | Ang           |                | -         |  | Sep Data-Time                              | DataTime                                 | New    |     |
|    |  |  |                         |              |               |                |               | 105              |                | 100          |                |                    |            |             |               | -Bastari -     |           |  |  |  |        | 10  |

- Permeability ~ 15 md, Skin Is Low And Remains Constant
- Reservoir Pressure Drops 6000 psia
- Reservoir Appears To Be In Depletion Drive

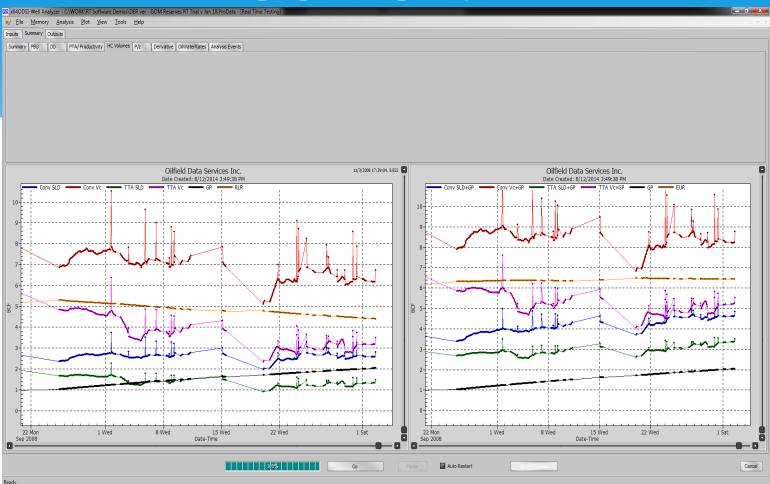


- No Major Shifts In Productivity (No Shifts In Scalar Value Or Slope)
- Inverse Productivity indicates Pseudo Steady-State Response



• P/Z Calculation and SLD-P Calculation Gives Us 4-10 BCF

Slide 163



- Running Energy And Material Balances
- LHS: Remaining Apparent Gas Volume
- RHS: Total Gas Volume
- This can be Compared With P/Z Results

#### GOM Shelf – Static and Flowing MBALS

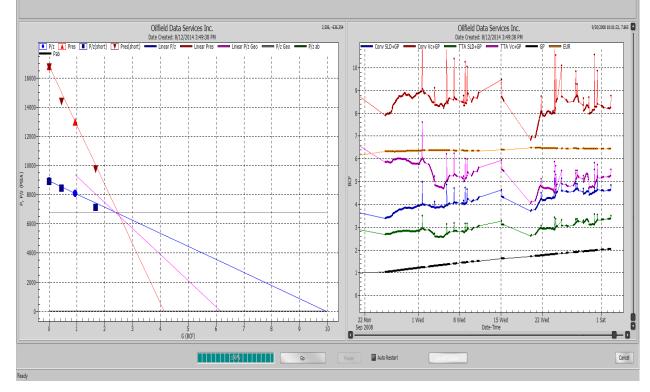
| 64ODSI-Well Analyzer - C | WORK\RT Soft                            |                   |             |               |                |  |                                       |              |                       |                     |                           |            |  |             |  |
|--------------------------|---|-------------------|-------------|---------------|----------------|--|---------------------------------------|--------------|-----------------------|---------------------|---------------------------|------------|--|-------------|--|
| PT 14 1 1                |   |                   |             | OM Reserves F | RT Trial v Jan | 18.ProData - [Real Tin                 | ne Testing]                           |              | _                     |                     | _                         |            |  |             |  |
| <u>File Memory Analy</u> | ysis <u>P</u> lot <u>V</u>              | iew <u>l</u> ools | Help        |               |                |  |                                       |              |                       |                     |                           |            |  |             |  |
| uts Summary Outputs      |   |                   | (F111)      |               |                |  |                                       |              |                       |                     |                           |            |  |             |  |
|                          | PTA/ Productivit                        | -                 |             | 1             |                | Analysis Events                        | :                                     |              |                       |                     |                           |            | :  |             |  |
| ate Time                 |   | PBU<br>Duration   | Pres        | z-Factor      | P/z            | GIP SLD @P=0                           | GIP SLD<br>@P ab=15                   | GIP P/z @P=0 | GIP P/z<br>@P/z ab=15 | GIP P/z geo<br>@P=0 | GIP P/z geo<br>@P/z ab=15 | m Pres     | m Pz   | m Pz<br>Geo |  |
| IM/dd/yyyy HH:mm:        | ss BCF                                  | HOURS             | PSIA        | dimless       | PSIA           | BCF                                    | BCF                                   | BCF          | BCF                   | BCF                 | BCF                       | PSIA/BCF   | PSIA/BCF   | PSIA/BC     |  |
| 1/01/0001 00:00          | :0 0.000                                |                   | 16800       | 1.883         | 8922.6         |  |                                       |              |                       |                     |                           |            |  |             |  |
| 3/03/2008 09:55:00       | 0.005                                   | 6                 | 16728       | 1.878         | 8908.94        |  |                                       |              |                       |                     |                           |            |  |             |  |
| 8/15/2008 16:49:00       |   | 7                 | 14374       |               | 8419.16        |  |                                       |              |                       |                     |                           |            |  |             |  |
| 9/22/2008 17:01          |   | 267               | 13009       |               | 8088.4         |  | 4.1                                   | 10.0         | 10.0                  | 6.2                 | 6.2                       | -4062.3    | - <b>893.9</b>   | -1787.      |  |
| 0/18/2008 12:37:00       | 1.667                                   | 33                | 9759        | 1.374         | 7101.35        | 4.1                                    | 4.1                                   | 10.0         | 10.0                  | 6.2                 | 6.2                       | -4062.3    | -893.9   | -1787.9     |  |
|                          |   |                   |             |               |                |  |                                       |              |                       |                     |                           |            |  |             |  |
|                          |   |                   |             |               |                |  |                                       |              |                       |                     |                           |            |  |             |  |
|                          |   |                   |             |               |                | ervices Inc.<br>2014 3:49:38 PM        |                                       |              | 2.506, -636           | .354                |                           |            | Oilfield Data<br>Date Created: 8/12  |             | 9/30/2008 10:01:32, 7                  |
| P/z A                    | Pres 🔳 P/z(                             | short) 💌 F        | Pres(short) | Lin           | ear P/z        | Linear Pres                            | Linear P/z Geo                        | P/z Geo      | P/z ab                |                     | Conv SLD+GP               | Conv Vc+GP | TTA SLD+GP   | TTA Vc+GP   | GP EUR                                 |
| F 🕌                      |   | 1                 |             |               |                |  | 1                                     |              |                       | 10                  |                           |            | j  |             |  |
| 5000                     |   |                   |             |               |                |  |                                       |              |                       |                     |                           |            |  | 4           |  |
|                          |   |                   |             |               |                |  |                                       |              |                       | 9                   |                           |            |  |             |  |
| 4000                     |   |                   |             |               |                |  |                                       |              |                       |                     | ~~~                       | Nat        | the fill the second sec |             |  |
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| вооо                     | · • • • • • • • • • • • • • • • • • • • |                   |             |               |                | · <del> </del>                         | ·                                     |              |                       |                     |                           |            | 1 . have   |             | Jun                                    |
| F                        |   |                   |             |               |                |  |                                       |              |                       | 4+-+                |                           |            |  |             |  |
| 6000                     |   |                   |             |               |                | ·                                      | · · · · · · · · · · · · · · · · · · · |              |                       |                     |                           |            | 1 11   |             | 1 produced                             |
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| 2000                     |   |                   |             |               |                |  |                                       |              |                       |                     |                           |            |  |             |  |
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|                          | 1                                       | 2                 | 3           | 4             |                | 5 6                                    | 7                                     | 8 9          | 10                    | Sep 2008            | 1                         |            | Date   | -Time       | 1 Jal                                  |
|                          |   |                   |             |               | G              | (BCF)                                  |                                       |              |                       |                     |                           |            |  |             |  |
|                          |   |                   |             |               |                |  | 100%                                  |              | Go                    | Pause               | Auto Restart              | SaveDTC    | lumn   |             | Ca                                     |
|                          |   |                   |             |               |                |  |                                       |              |                       |                     |                           |            |  |             |  |

🗱 x640DSI-Well Analyzer - C:\WORK\RT Software Demos\DER ver - GOM Reserves RT Trial v Jan 18.ProData - [Real Time

• LHS:

- SLD/Straight Line
   Depletion (Red)
- P/Z
   Expansion/Depletion:
   (Blue)
- RHS:
  - Conventional Expansion: (Red)
  - Conventional SLD: (Blue)
  - TTA Compressibility: (Purple)
  - TTA SLD: (Green)
  - Gp: Black
  - Static MBAL To The Gas/Water Contact: (Orange)

| Summary PBU DD PT   | A/ Productivity | [UC Values]     | 0/2   |          |         | Analysis Events |                     |              |                       |                     |                           |          |          |             |
|---------------------|-----------------|-----------------|-------|----------|---------|-----------------|---------------------|--------------|-----------------------|---------------------|---------------------------|----------|----------|-------------|
|                     | 1               | :               | •     |          | 1       |                 |                     |              |                       |                     |                           |          |          |             |
| Date Time           |                 | PBU<br>Duration | Pres  | z-Factor | P/z     | GIP SLD @P=0    | GIP SLD<br>@P ab=15 | GIP P/z @P=0 | GIP P/z<br>@P/z ab=15 | GIP P/z geo<br>@P=0 | GIP P/z geo<br>@P/z ab=15 | m Pres   | m Pz     | m Pz<br>Geo |
| MM/dd/yyyy HH:mm:ss | BCF             | HOURS           | PSIA  | dimless  | PSIA    | BCF             | BCF                 | BCF          | BCF                   | BCF                 | BCF                       | PSIA/BCF | PSIA/BCF | PSIA/BC     |
| 01/01/0001 00:00:0  | 0.000           |                 | 16800 | 1.883    | 8922.6  |                 |                     |              |                       |                     |                           |          |          |             |
| 08/03/2008 09:55:00 | 0.005           | 6               | 16728 | 1.878    | 8908.94 |                 |                     |              |                       |                     |                           |          |          |             |
| 08/15/2008 16:49:00 | 0.445           | 7               | 14374 | 1.707    | 8419.16 |                 |                     |              |                       |                     |                           |          |          |             |
| 09/22/2008 17:01:0  | 0.933           | 267             | 13009 | 1.608    | 8088.4  | 4.1             | 4.1                 | 10.0         | 10.0                  | 6.2                 | 6.2                       | -4062.3  | -893.9   | -1787.      |
| 10/18/2008 12:37:00 | 1.667           | 33              | 9759  | 1.374    | 7101.35 | 4.1             | 4.1                 | 10.0         | 10.0                  | 6.2                 | 6.2                       | -4062.3  | -893.9   | -1787.9     |



#### **GOM Shelf HP-HT Conclusions**

- \* Skin & Perm are fluctuating due to crossflow and differential depletion in high-perm zones
- \* Moderate Perm with Low Skin
- \* Gas on top of dead-leg water

Reservoir Volume: 10 BCF of potential elastic energy

- \* 3 BCF of water (dead leg)
- \* 1.5 BCF of rock compaction
- \* 5.5 BCF of Mobile Gas
- \* 1.0 BCF of "Tight" Gas

#### Notes on the Case Studies:

At no time was the pressure data "smoothed" At no time was the data forced to fit a model At no time was the "answer" provided ahead of time

If you let it, the well will tell you what it's volume is made of and what it can produce

Analyze the Data Without Imposing Bias!

# Thoughts, Musings & Conclusions

#### What is Good Oilfield Management?

- \* Maximize NPV
- \* Maximize Recoverable Reserves
- \* Avoid waste (time/money/resources)
- \* Mitigate/minimize risk (Ops/Reserves/HSE)
- \* Learn from your mistakes (and successes)
- MAKE BETTER DECISIONS IN A TIMELY FASHION

#### What is BAD Oilfield Management?

- Maximize bonus
- \* Maximize 'booked' reserves
- \* The INSIDE View eliminate/ignore contrary data
- \* Falling in love with a rate
- \* Wait until a problem is obvious (and expensive to fix)
- Hope no one notices (until you've moved on) make sure no one takes ownership
- \* Shoot the messenger
- Make the decision that's best for you, not the company

# What are the Consequences of Automated Monitoring/Surveillance?

- Democratized information/results
  - \* Can spend time discussing what it means
  - \* Easier to translate to other departments/silos
  - \* Less finger pointing and more inclusive work processes
- \* Quicker Decisions
  - Reach conclusions on what it means
  - \* Easier to focus on NPV of Decisions
- \* Quicker Actions/Inactions

#### **Conclusions: RT Well Evaluation**

- Proper Instrumentation and Visualization Software are the 1<sup>st</sup> Step (Don't Drop Bits!)
- \* Closed-Loop Solutions for the Wellbore and Reservoir make it possible to quickly check system model
- \* Do NOT impose a "static" model on the well
- Warning an Engineer when (or before) something bad happens is more important than being accurate to the 9<sup>th</sup> decimal place
- \* Checking the results of an Automated Calculation is a lot easier and more timely than doing it yourself

## Final Thoughts

- \* This technology is already here!
- Understand the physics not just the software package
- \* Always know:
  - \* How much MONEY is left in the ground?
  - \* How fast can I get it out (safely)
  - \* Is the performance changing?
- \* Compare NPV remaining vs. Cost of a "fix"
- \* Seek out non-biased results

# Chris Fair Oilfield Data Services, Inc. chris.fair@oilfielddataservices.com www.oilfielddataservices.com

March 30, 2016 Total - Pau